

# **Control and Operation of Multi-terminal VSC-HVDC**

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# Conclusions / Hypothesis

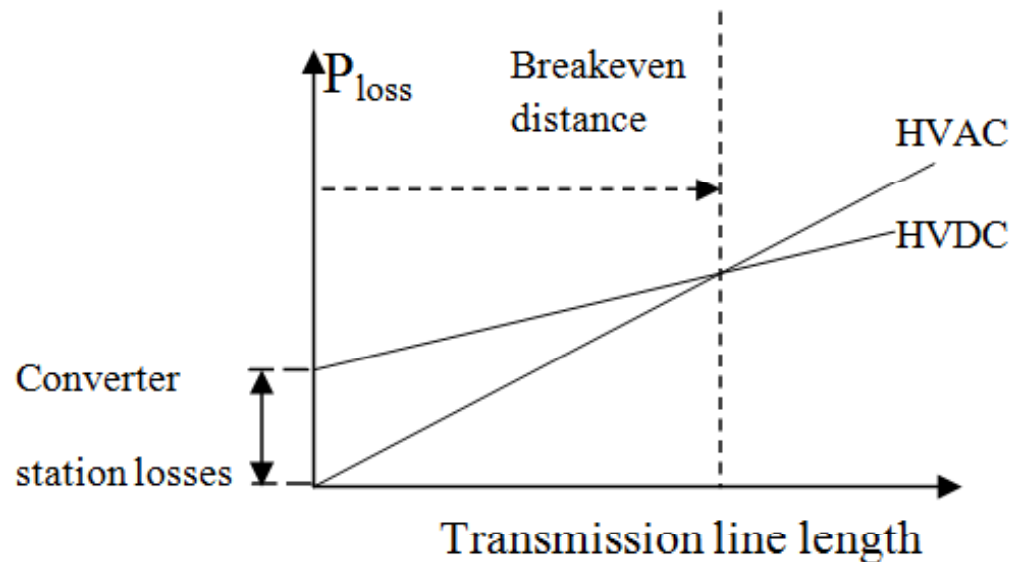
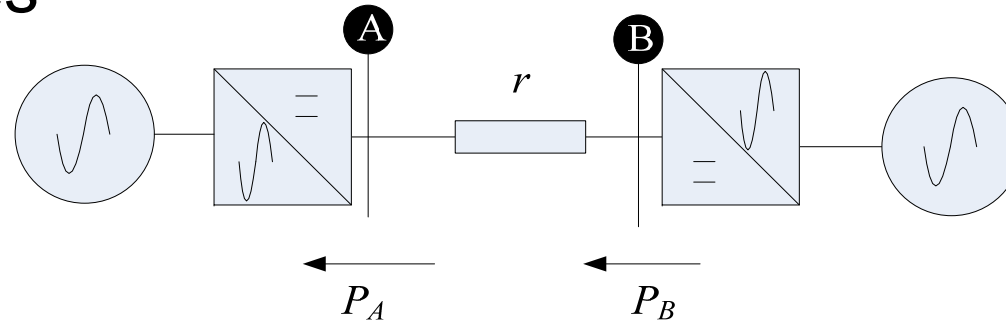
- *A meshed HVDC grid has the potential to improve security of supply!*
- A multi-terminal HVDC grid in the North Sea can effectively integrate the synchronous interconnections (UK, UCTE and Nordic)
- Can be operated as ONE control area (if desirable)
- Reserves (primary and secondary) can be shared without “technical constraints”
- Fast control and protection will enable network splitting to avoid risk of cascading outages and complete blackouts
- Fully integrate the power markets across the asynchronous areas.

# Outline

- Introduction: Why HVDC – VSC HVDC – Multi-terminal HVDC
- Power system security and Control objectives
- Modelling and control design
- Examples (illustrating security control aspects)

# HVDC Why?

1. To reduce total transmission loss for long distance power lines

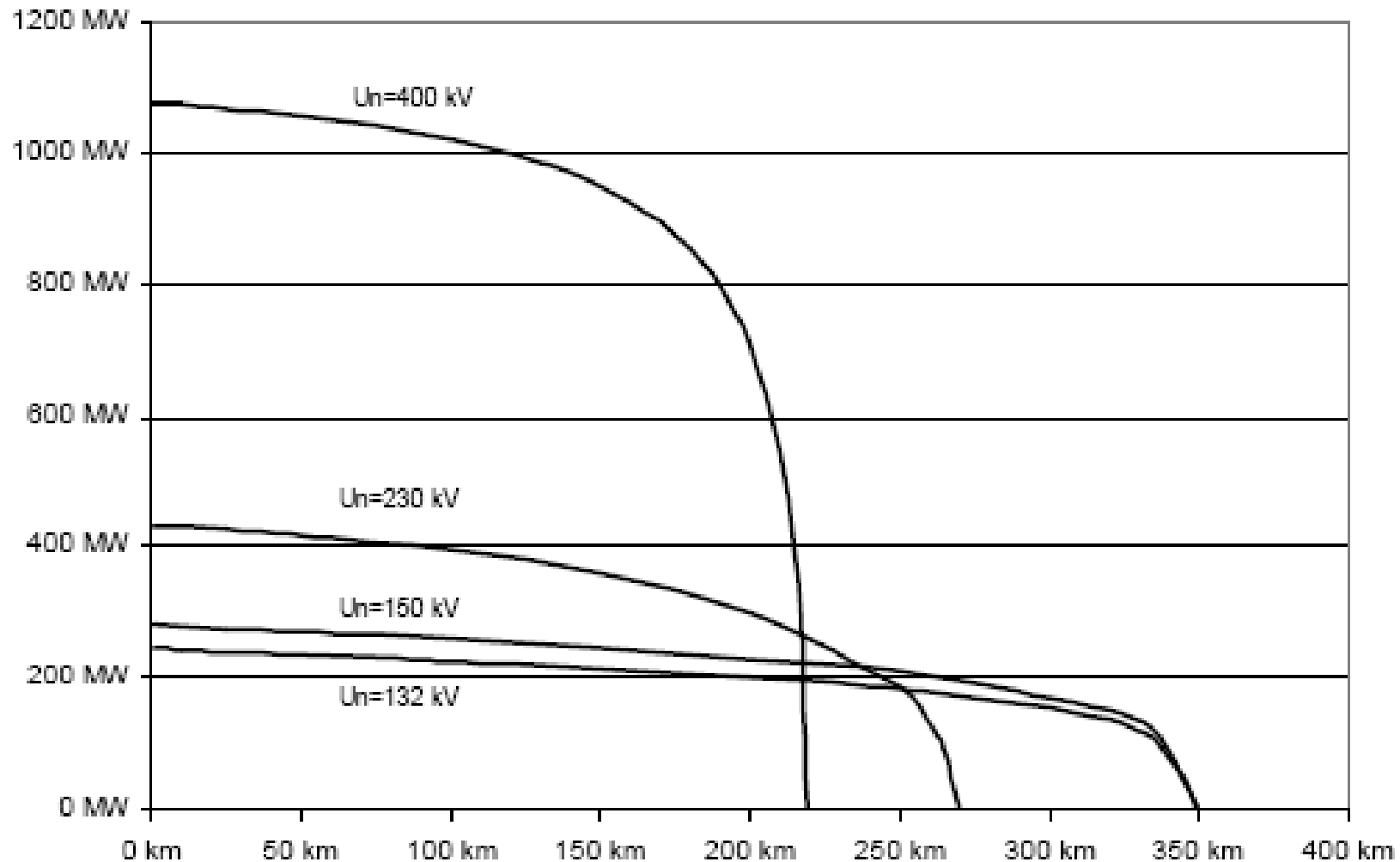


Break even distance for onshore application is about 600km and less than 100km for subsea transmissions

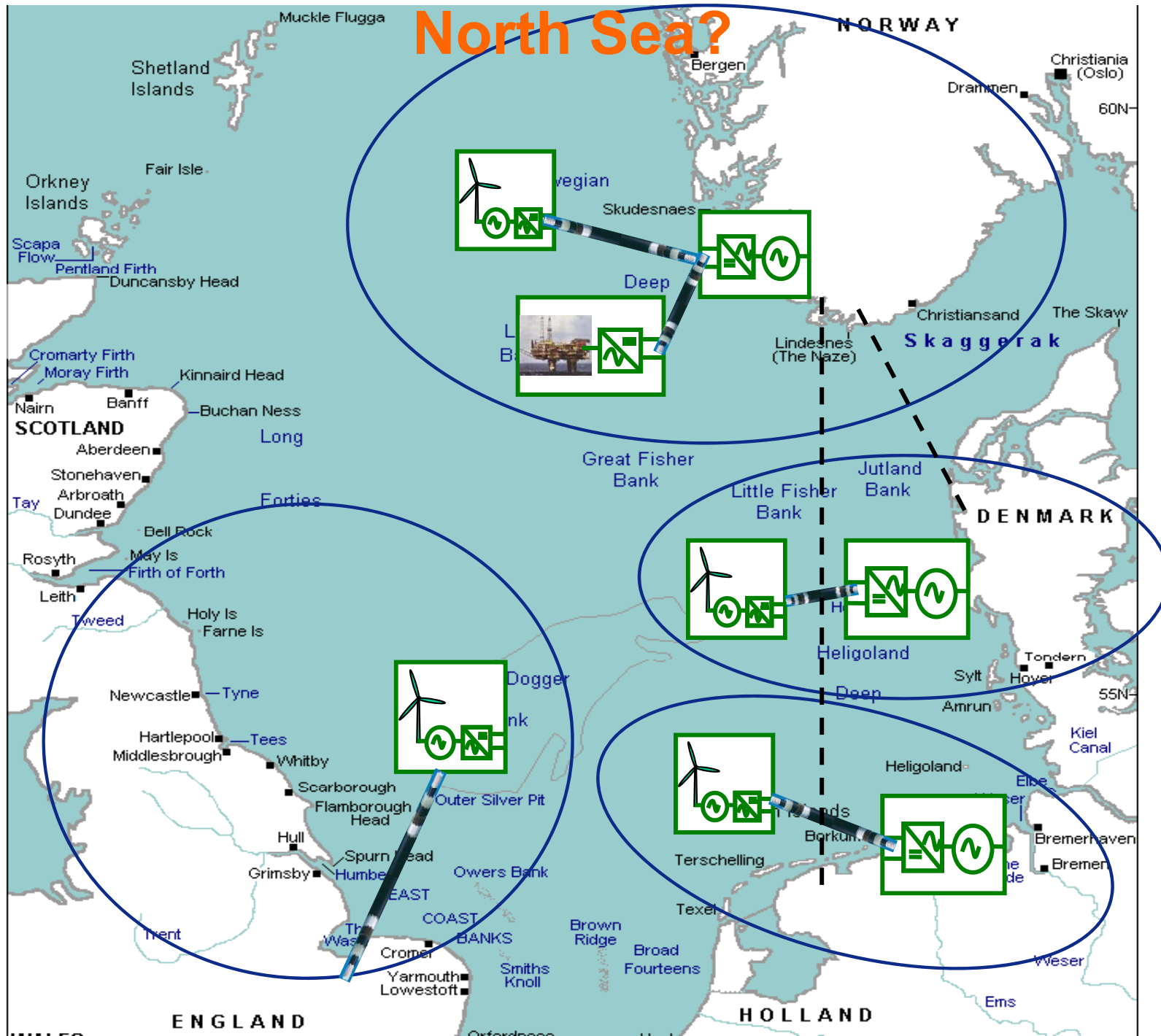
# Cont...

2. AC transmission becomes weak (unstable) for very large distances
3. Subsea power transmission
  - Large capacitive currents in AC cables severely limit the transmission capacity of long distance AC cables
  - The most common application area of HVDC is for subsea power transmission

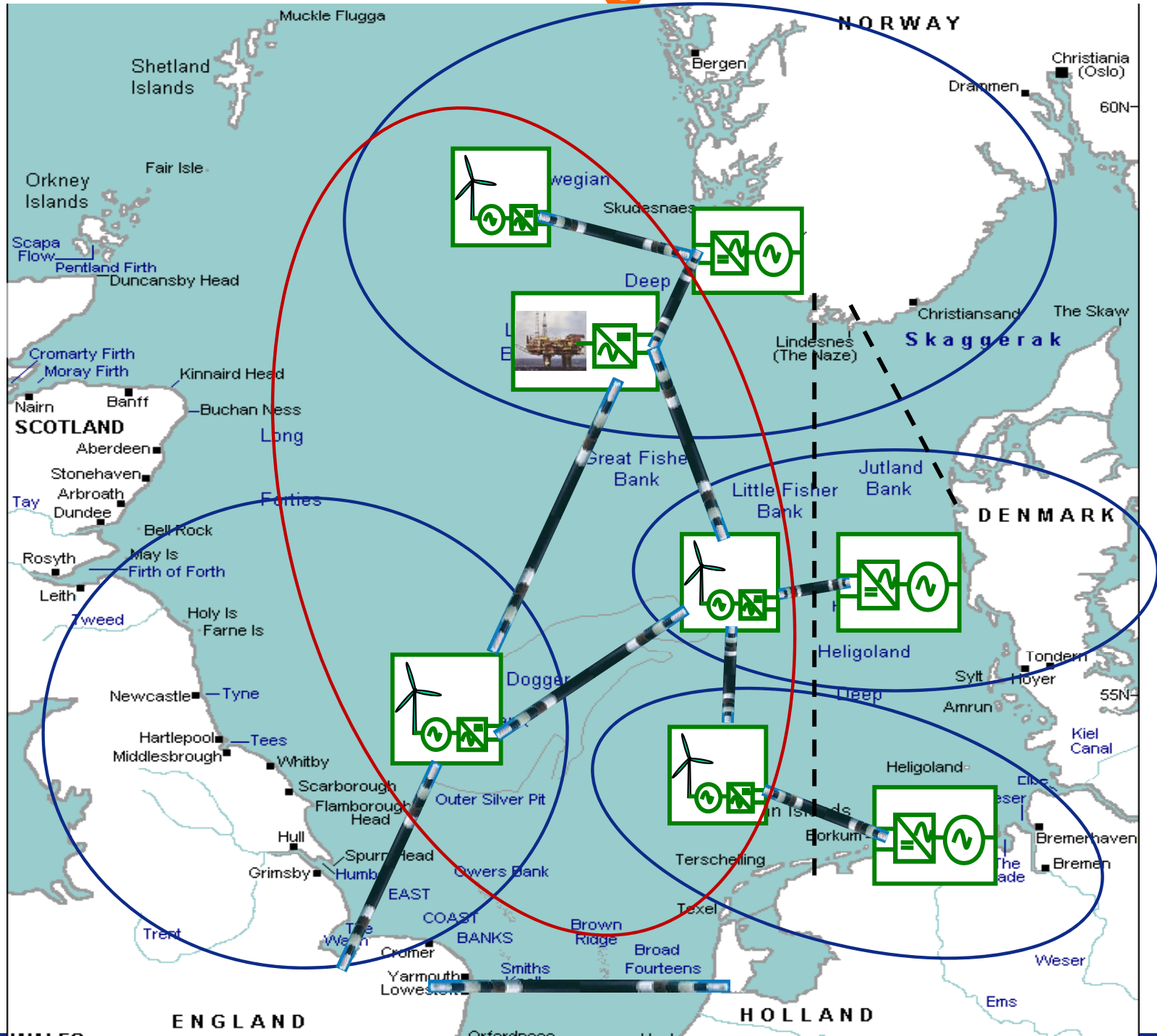
# Limits of transmission capacity, Submarine HVAC cables (ref Nexans)



# Why multiterminal VSC-HVDC (MTDC) in the North Sea?



# Grid integration





# Power system security

- Security standards: Deterministic (N-1) or risk based
- Ability to manage contingencies / outages:
  - Availability of reserves
  - Availability of transmission capacity
  - Stability and control

# Main challenges in operation and control

- Primary control:
    - Less primary reserves if new generation provide less frequency response
  - Secondary control:
    - More need for secondary reserves with more variable generation
  - Tertiary control:
    - Benefits with larger control areas and exchange of reserves.
- **New possibilities with an offshore Multi-terminal HVDC grid!**

# Control objectives: Desired operational capabilities

- Balancing of offshore wind power variation
- Resilience, e.g. to loss of a VSC-HVDC terminal ( $\approx$ load/generation loss) or line/cable
- Frequency response enhancement of AC grids
- Market integrated operation
- AC and DC fault handling capabilities

*Controllers should be designed to meet the requirements specified above.*

# Modelling:

## Active and Passive AC grid Connections

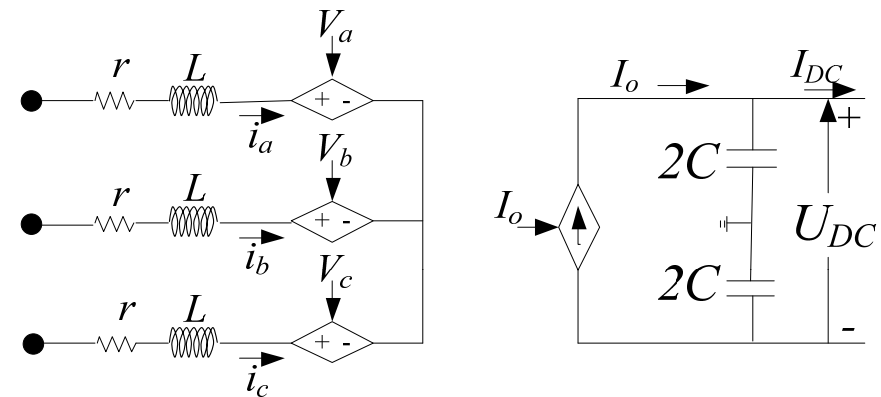
### Passive AC grid connection:

- AC voltage control at PCC
- no synchronization
- no control of current

### Active AC grid connection:

- Grid synchronization
- control of current flow

### Time-average VSC model

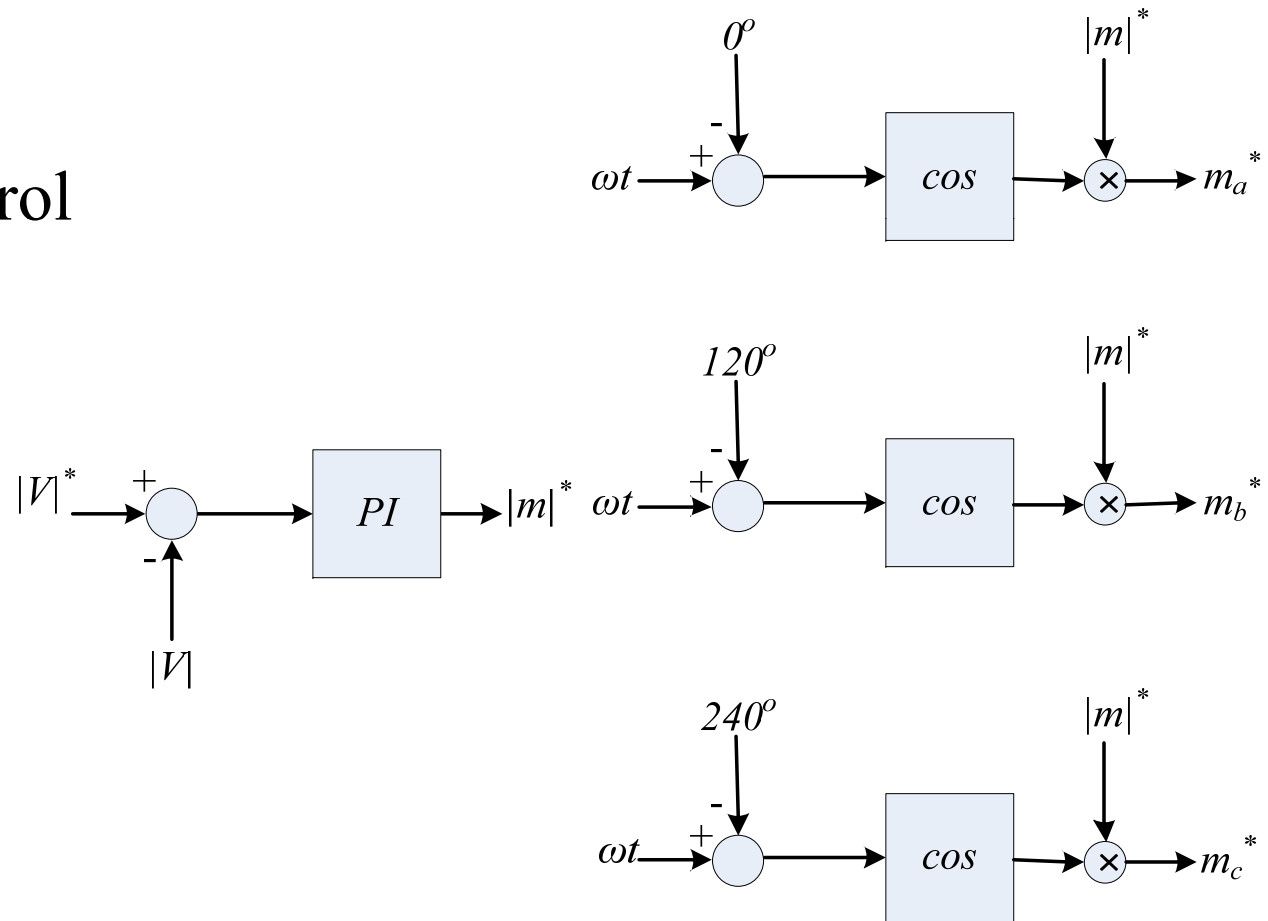


$$V_a = \frac{m_a U_{dc}}{2}, \quad V_b = \frac{m_b U_{dc}}{2}, \quad V_c = \frac{m_c U_{dc}}{2}$$

$$I_o = \frac{1}{2} (m_a i_a + m_b i_b + m_c i_c)$$

# Control of VSC Connected to Passive AC Grid

AC voltage control  
at PCC,  $|V|$



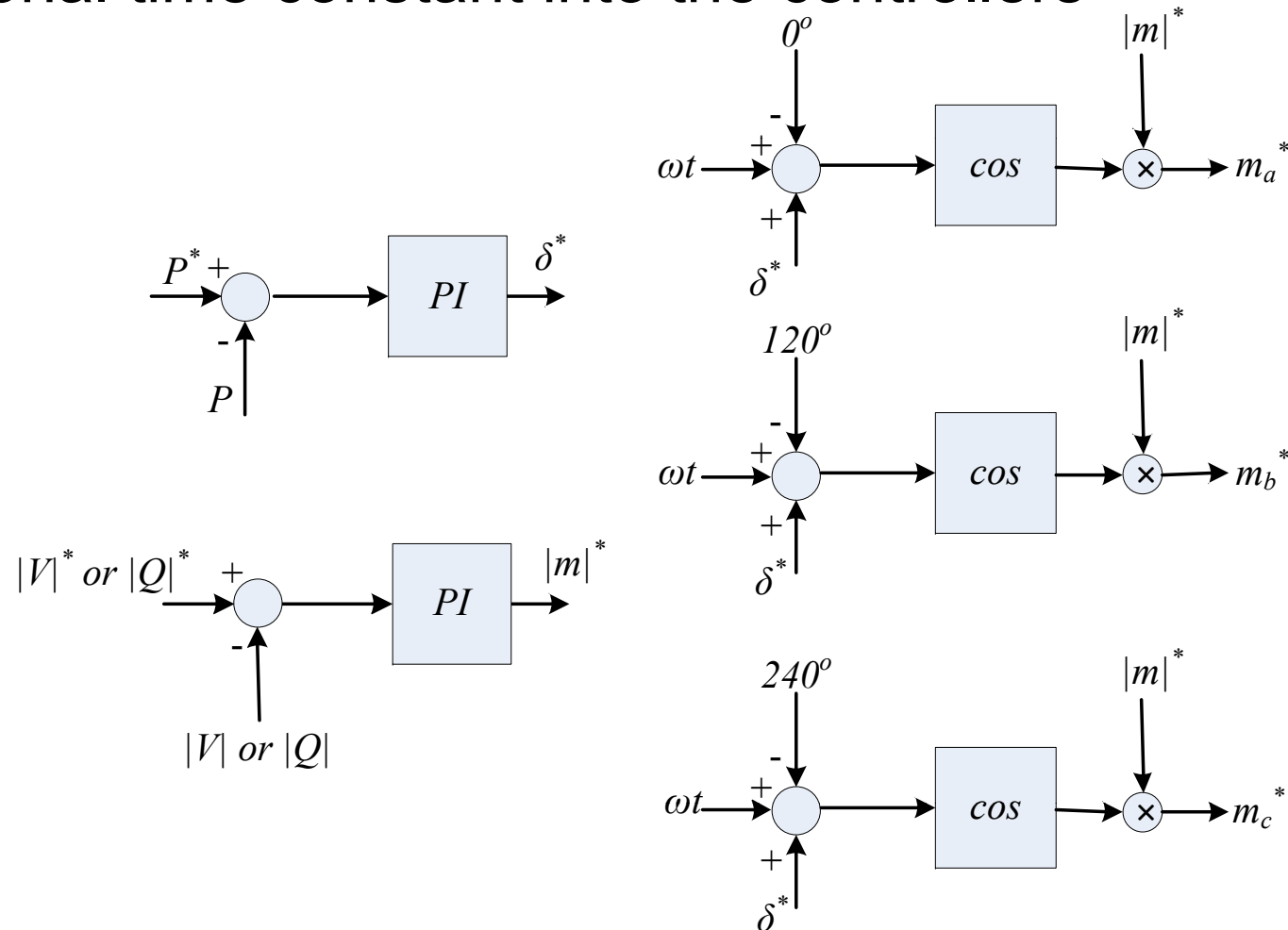
# Control of VSC Connected to Active AC grid

Two options:

- **$|m|$ ,  $\delta$  control**: uses phasor measurements
- ***decoupled axes (dq) control*** : uses instantaneous measurements

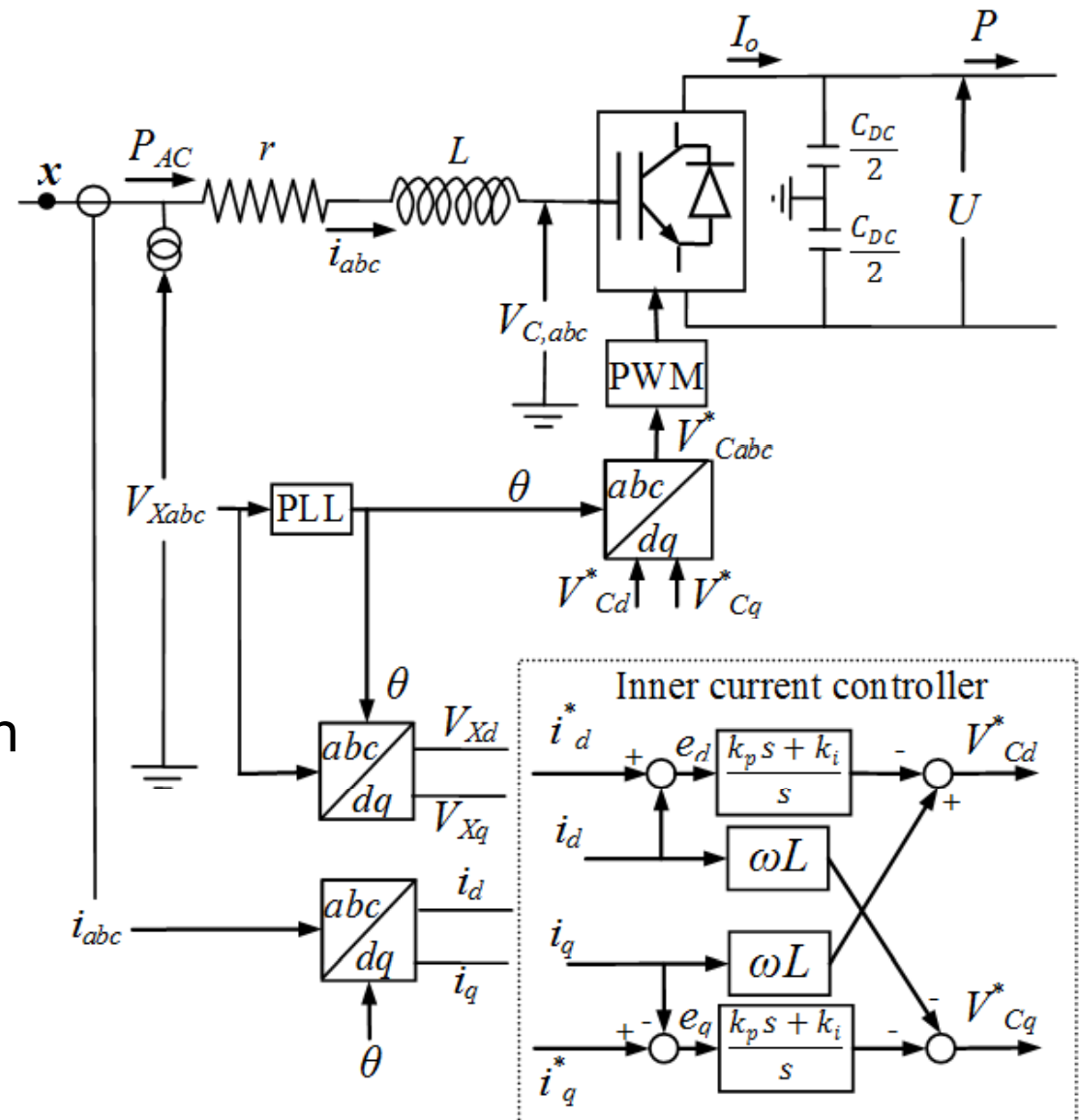
# $|m|, \delta$ control

- Suitable for modelling VSC control in phasor based electric power simulation tools (eg: DlgSILENT).
- Voltage and current phasor measurements introduce additional time constant into the controllers



# Decoupled axes ( $dq$ ) control

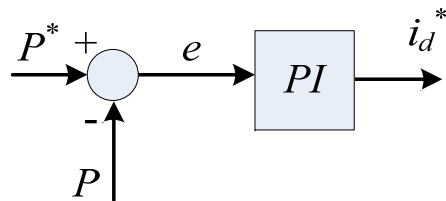
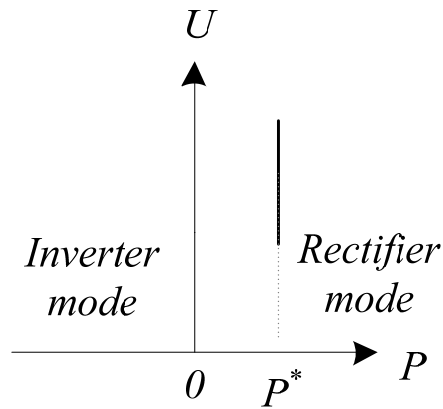
- Involves abc/dq transf.
- Fast control responses
- Mostly used in practice for VSC control
- Modelling is possible with electromagnetic transient softwares such as PSCAD



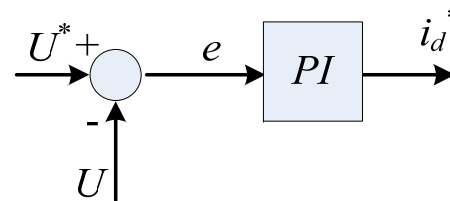
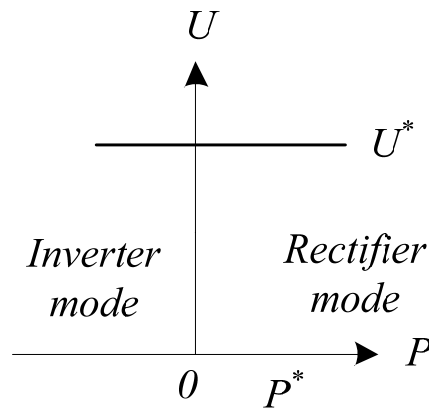


# Outer Controllers

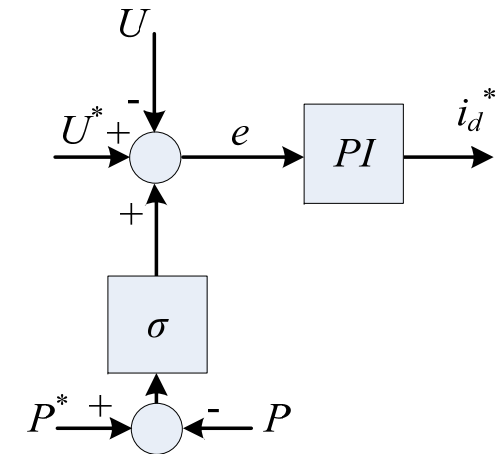
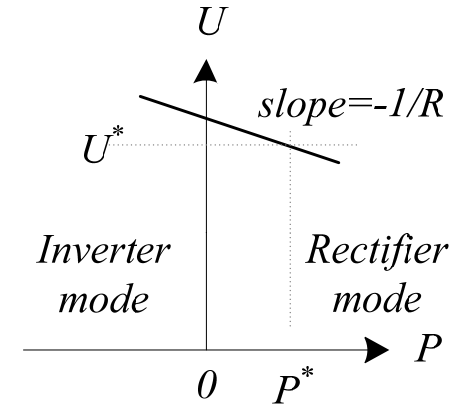
- Set the references to active & reactive (inner) current controllers
- Active power and/or DC bus voltage control (these types shown below)
- Reactive power and/or AC voltage control (not shown here)



**a. Fixed power control**



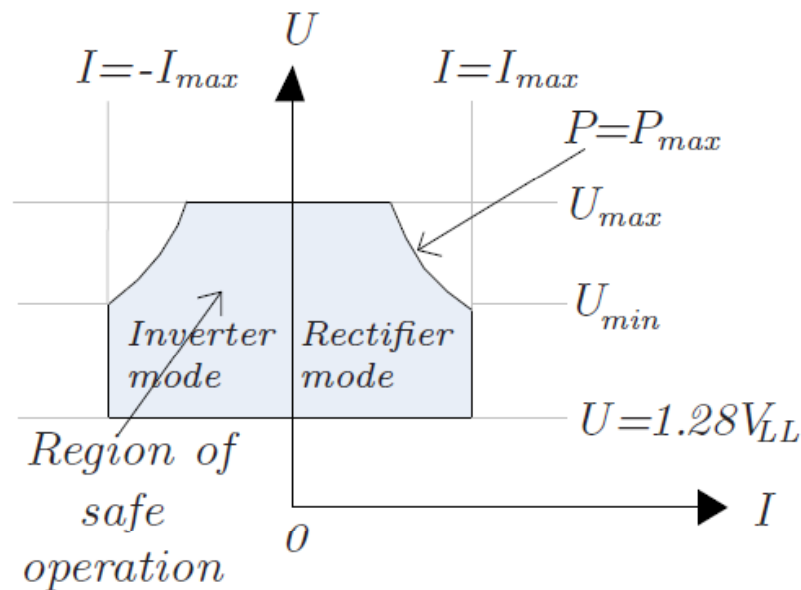
**b. Fixed DC voltage control**



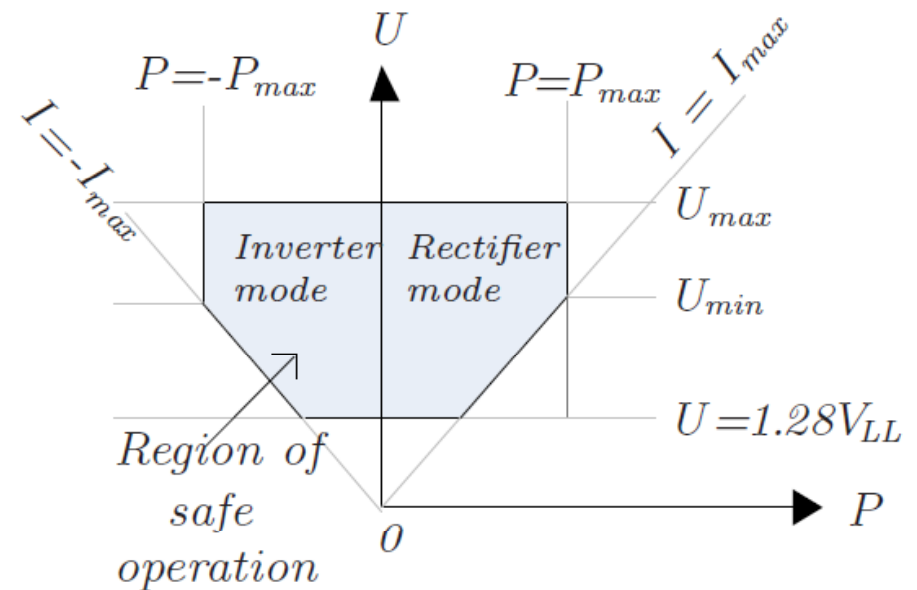
**c. DC voltage droop controller**

# Safe operating area of a VSC

Controller actions are limited within safe operating area



(a)

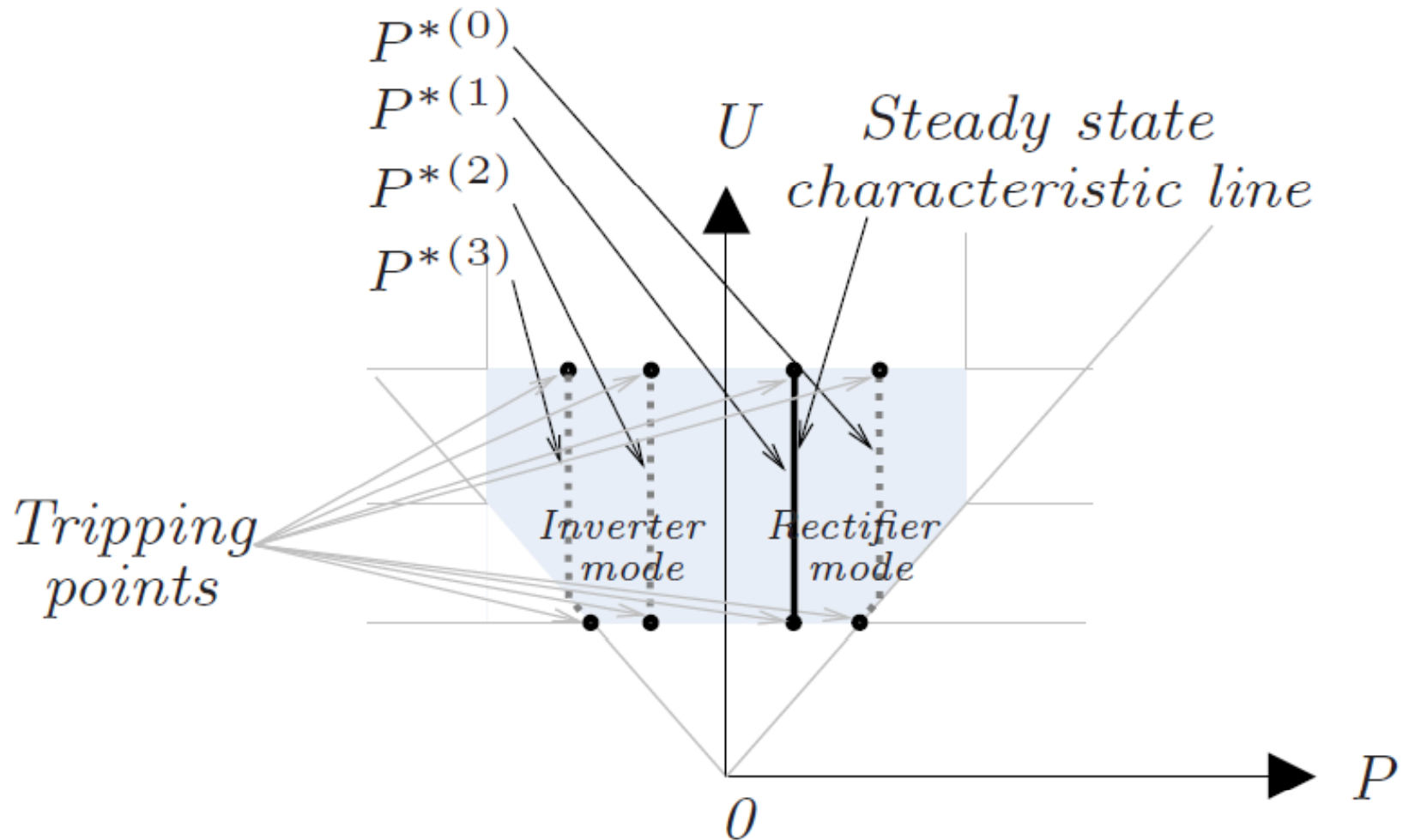


(b)

Safe operating area of a VSC: (a)  $U$  vs  $I$  safe operating region  
 (b)  $U$  vs  $P$  safe operating region

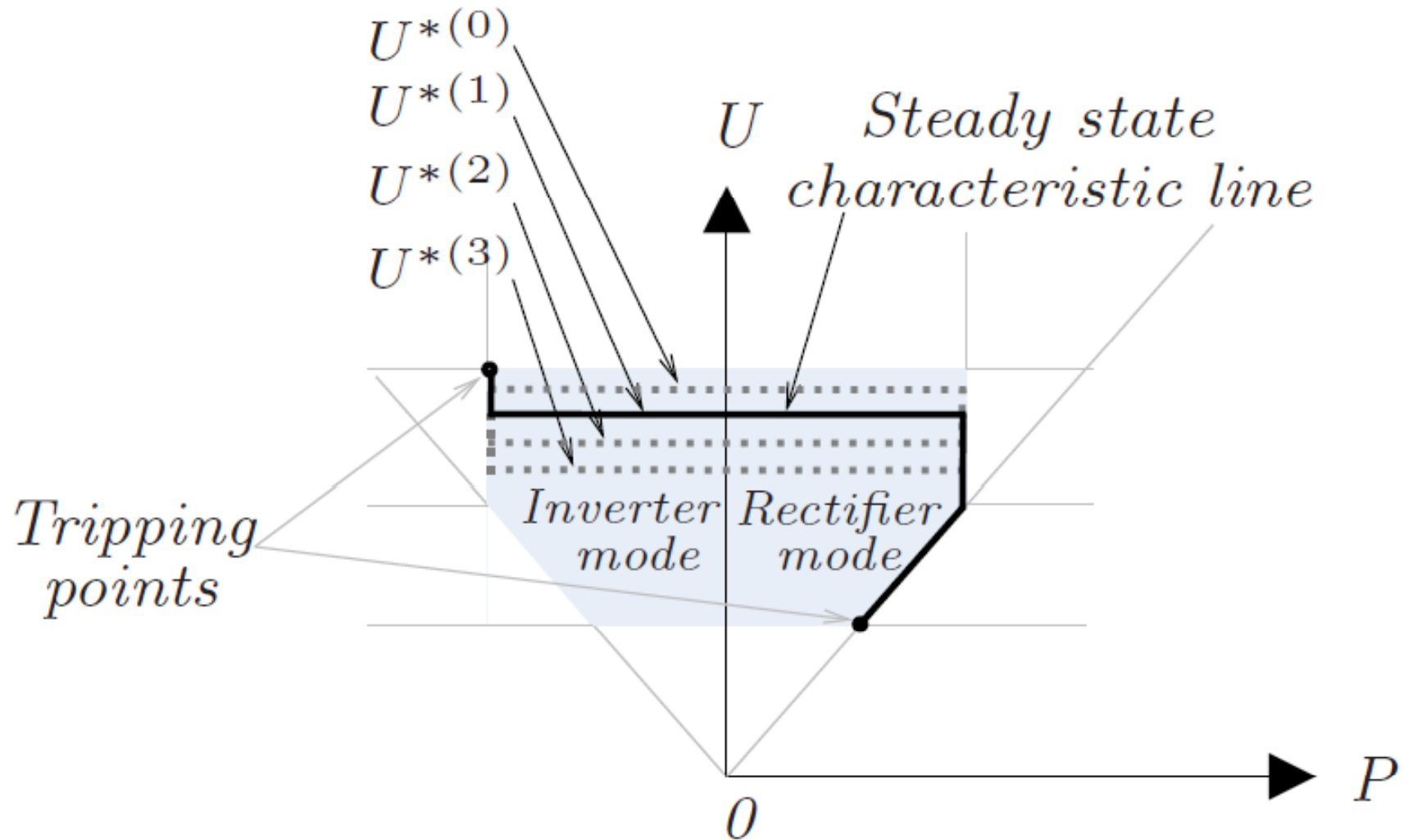
# Constant power control within the safe operating region

$P^*$  = power reference



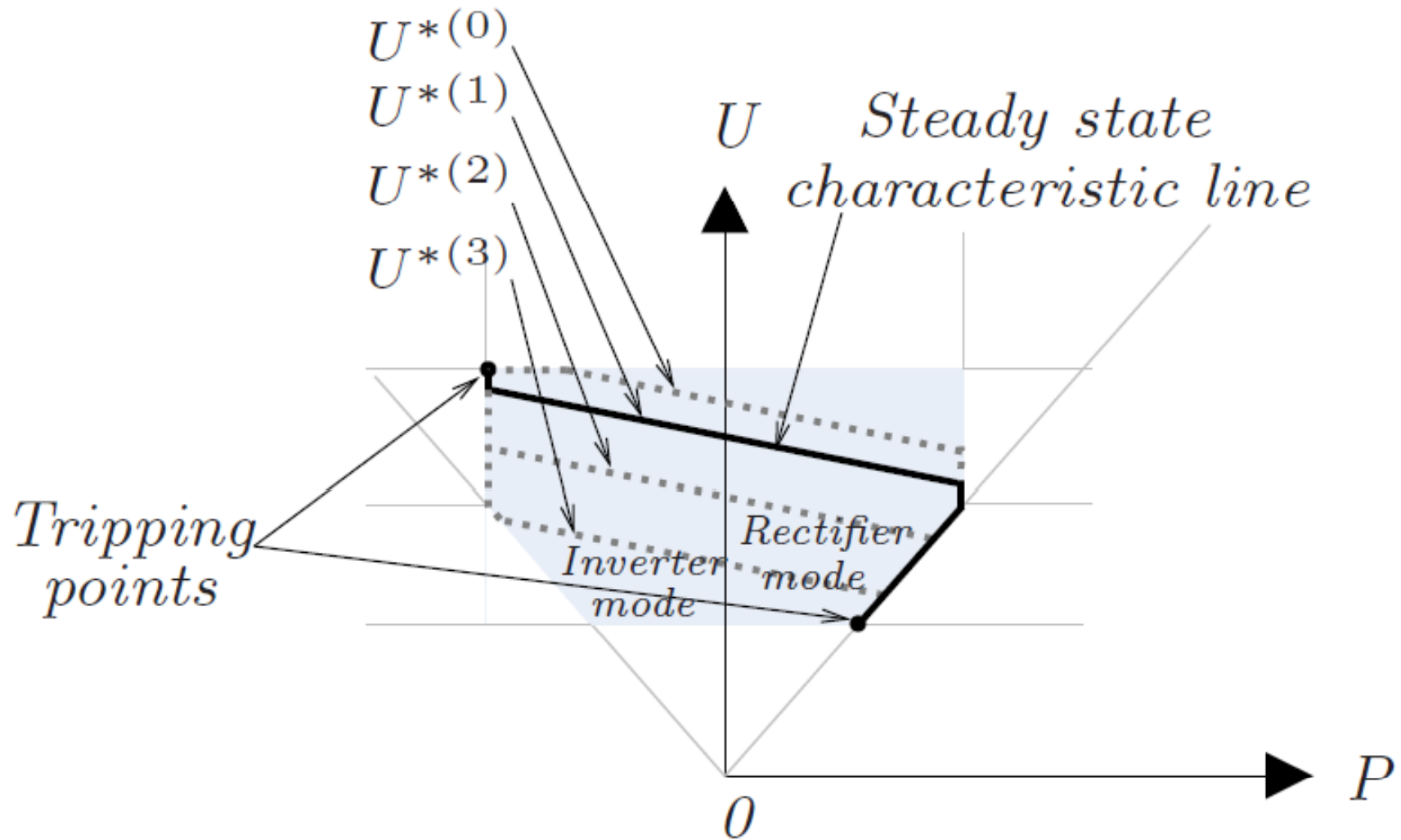
# Constant DC voltage control within the safe operating region

$U^*$  = DC voltage reference

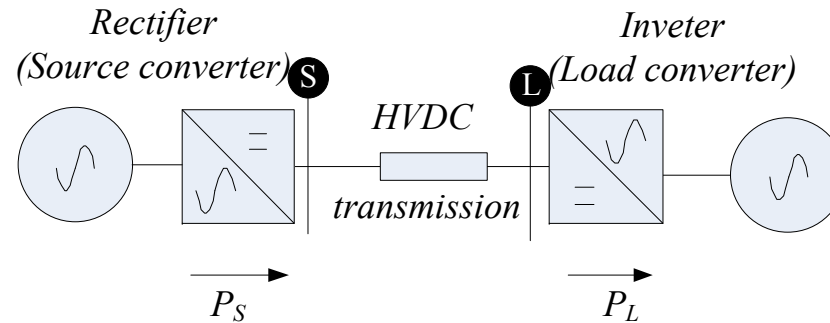


# DC voltage droop control within the safe operating region

$U^*$  = DC voltage reference



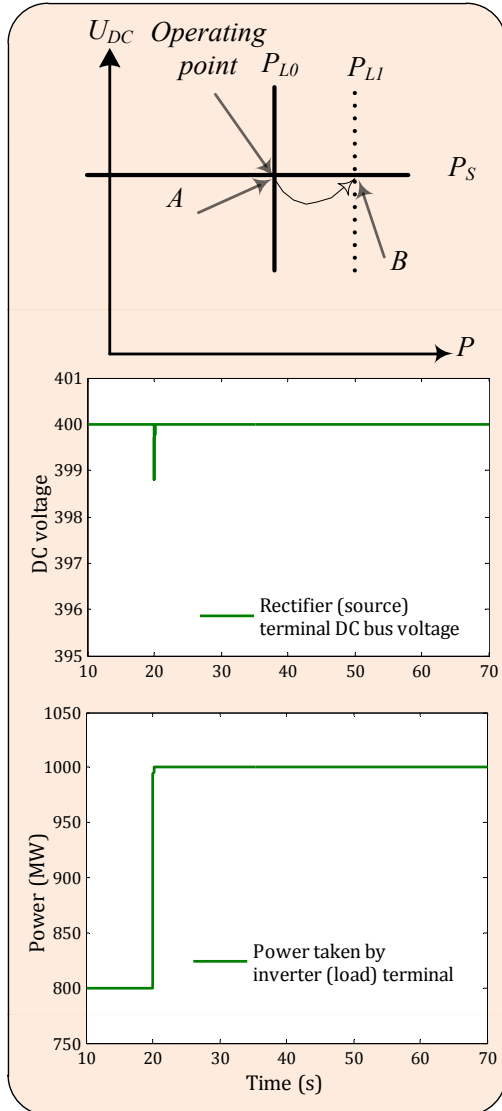
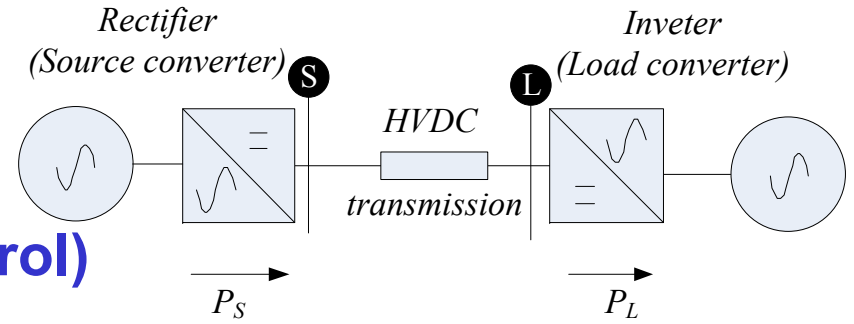
# Two terminal VSC-HVDC Control



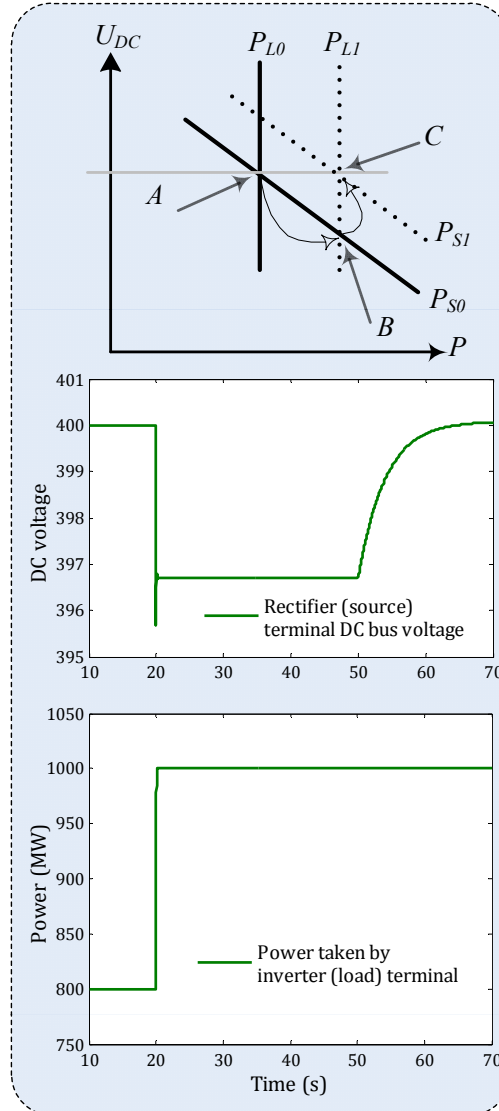
Control modes (3x3=9 combinations)		Remarks
Rectifier	Inverter	
Fixed power	Fixed power	X (Not viable)
Fixed power	DC Droop	√ (With risk of DC overvoltage)
Fixed power	Fixed DC voltage	√ (With risk of DC overvoltage)
DC Droop	Fixed power	√ (Good, P control by Inv.)
DC Droop	DC Droop	√ (Good, P control by Both)
DC Droop	Fixed DC voltage	√ (Good, P control by Rect.)
Fixed DC voltage	Fixed power	√ (Good, P control by Inv.)
Fixed DC voltage	DC Droop	√ (Good, P control by Inv.)
Fixed DC voltage	Fixed DC voltage	X (Not viable)

# DC Voltage Control Responses

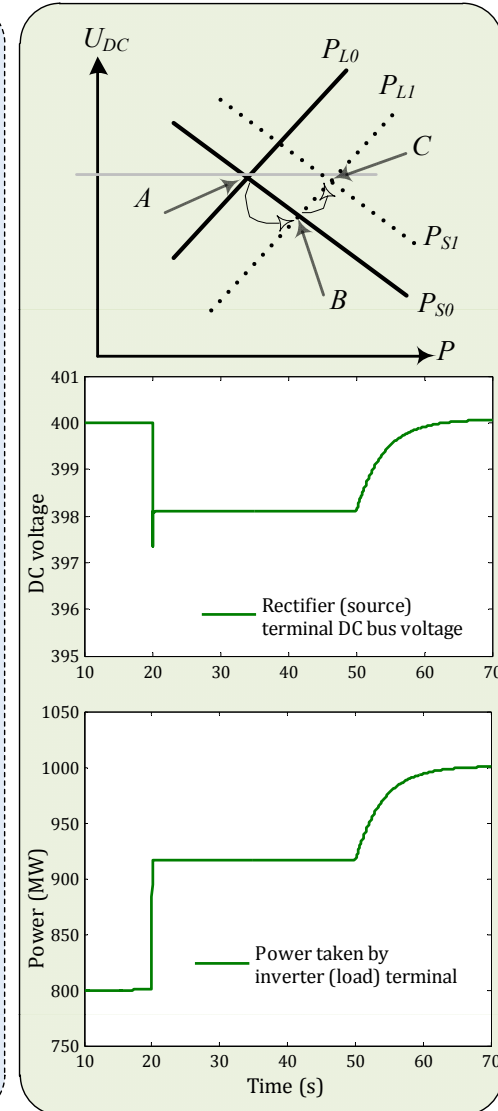
(Primary & secondary DC voltage control)



(a)

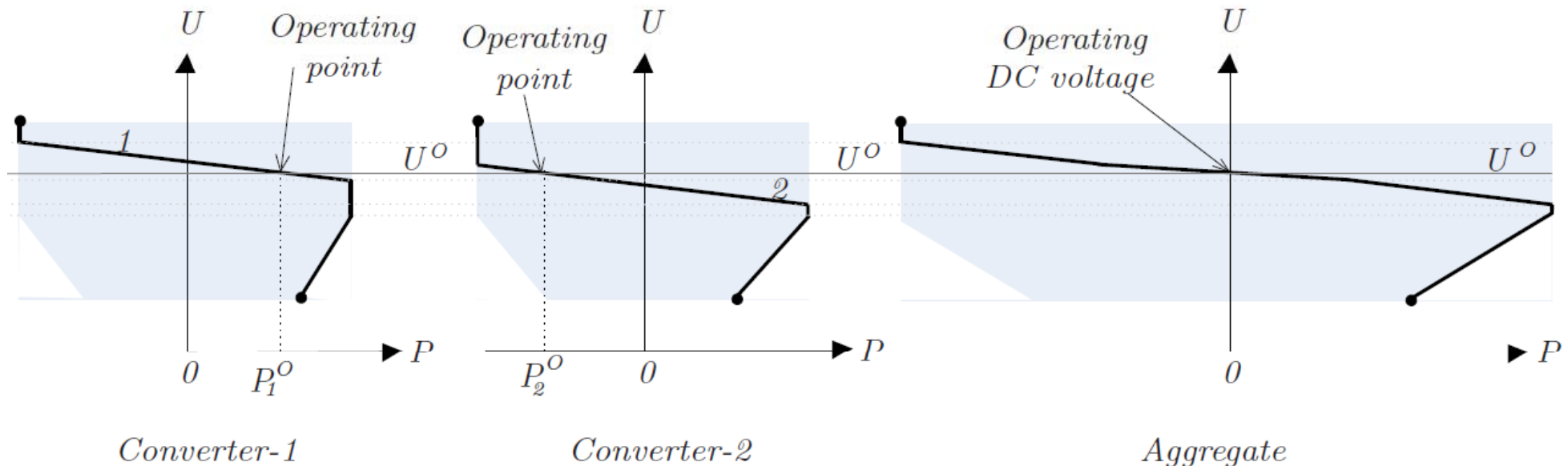


(b)



(c)

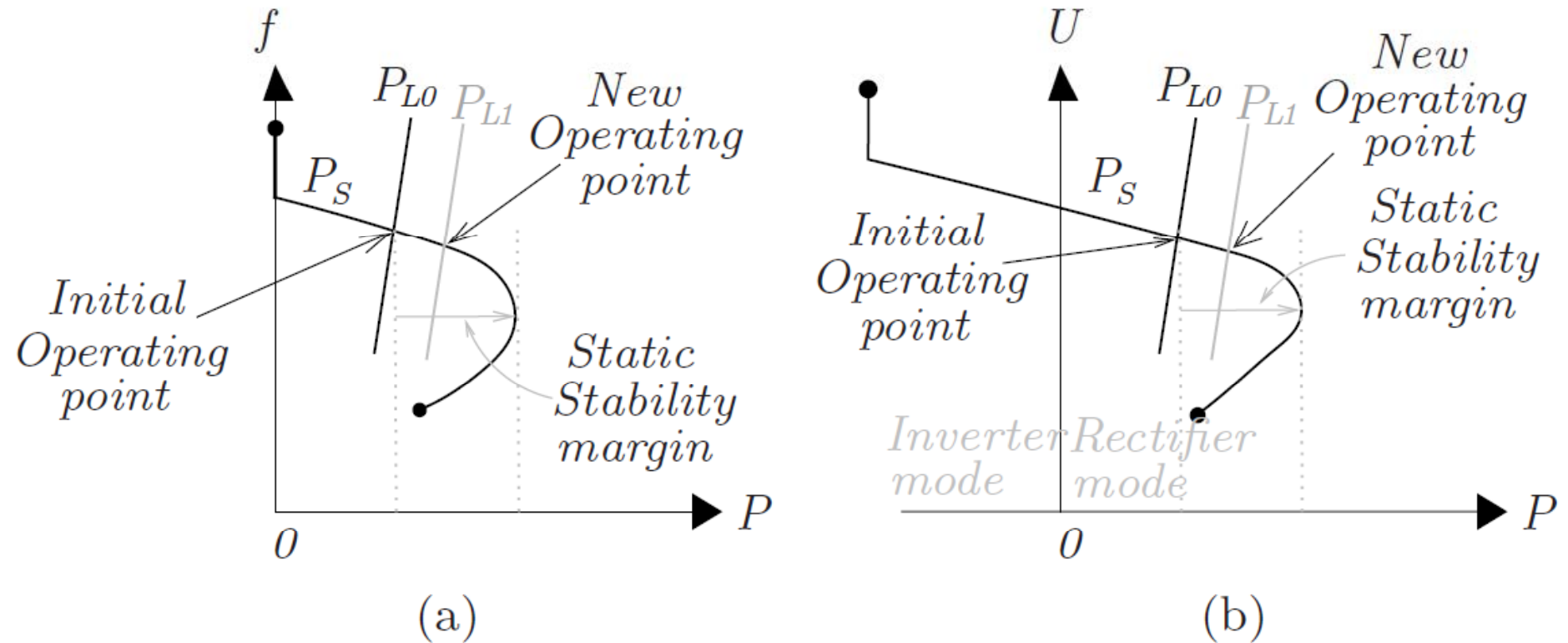
# Power flow control in DC grid : achieved by DC voltage droop



- No need for communication between terminals
- Many converter terminals contribute to DC voltage regulation
- DC analogy to distributed *frequency droop control* in AC systems

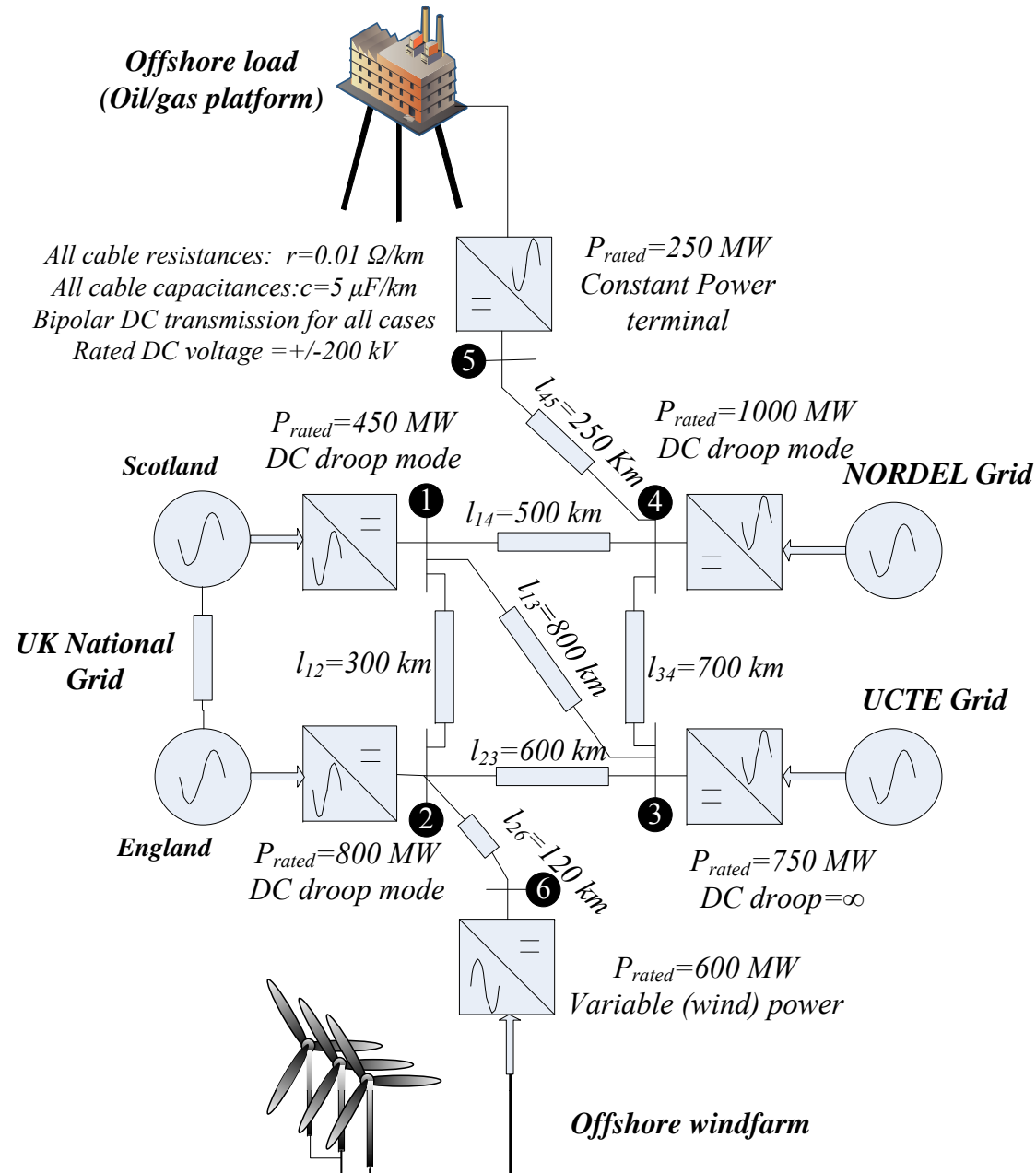


# Similarities of AC grid frequency droop control and DC voltage droop control of MTDC



Steady state characteristic of: (a) synchronous generator (b) VSC-HVDC terminal (The dots at the end of the characteristic lines show tripping points.)

# Test model: "North Sea DC grid"

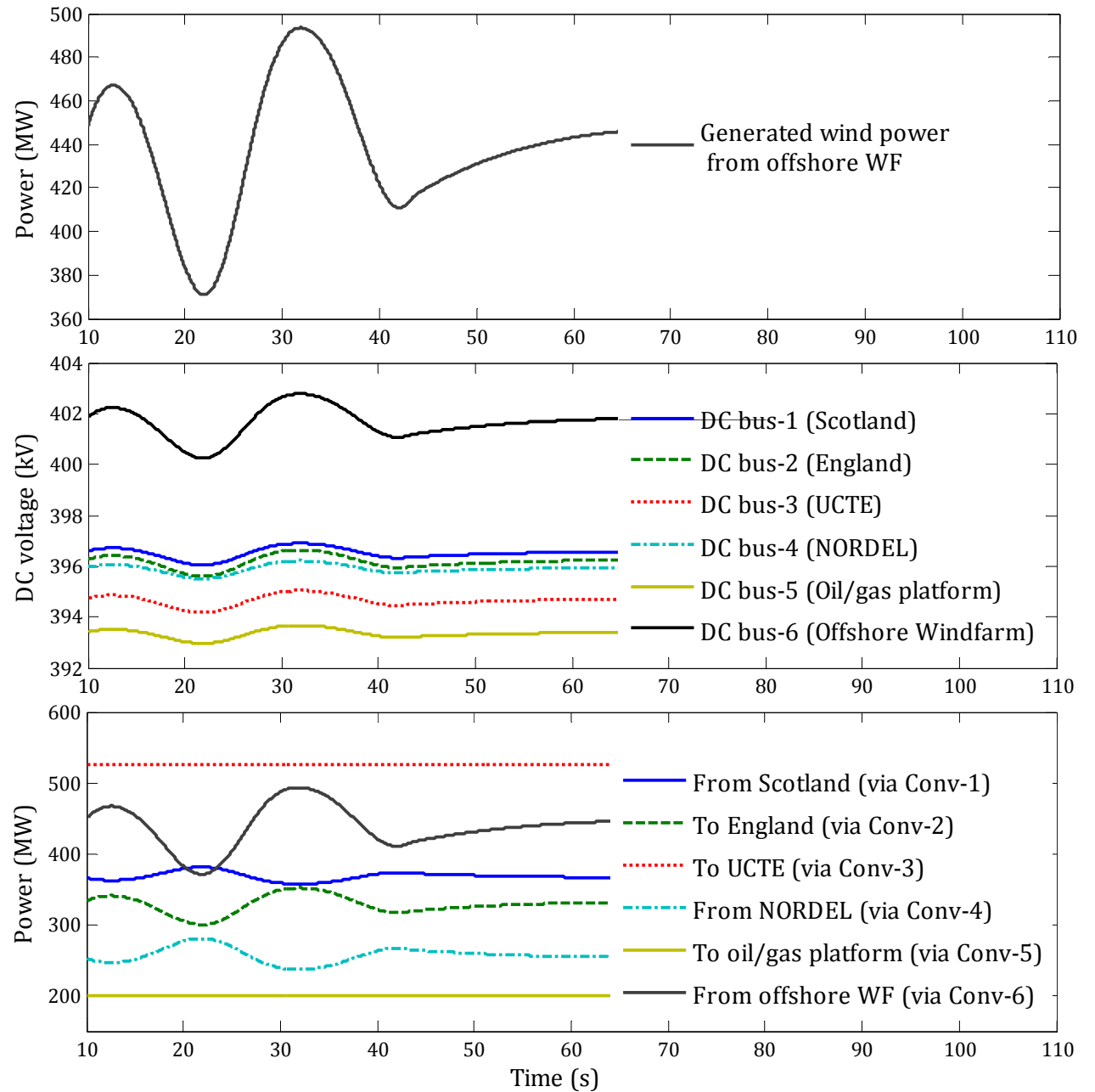
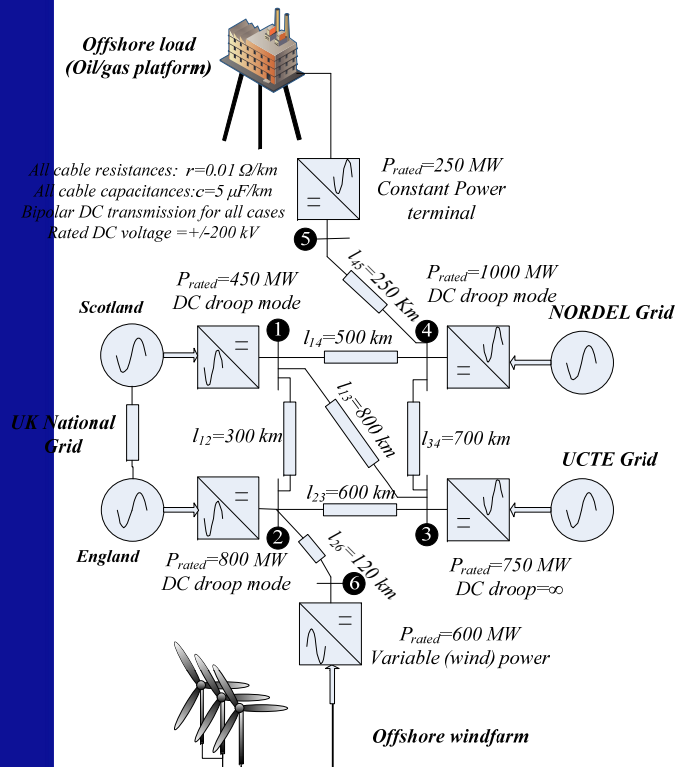


# Security analysis

## Examples illustrating security aspects related to operation and control

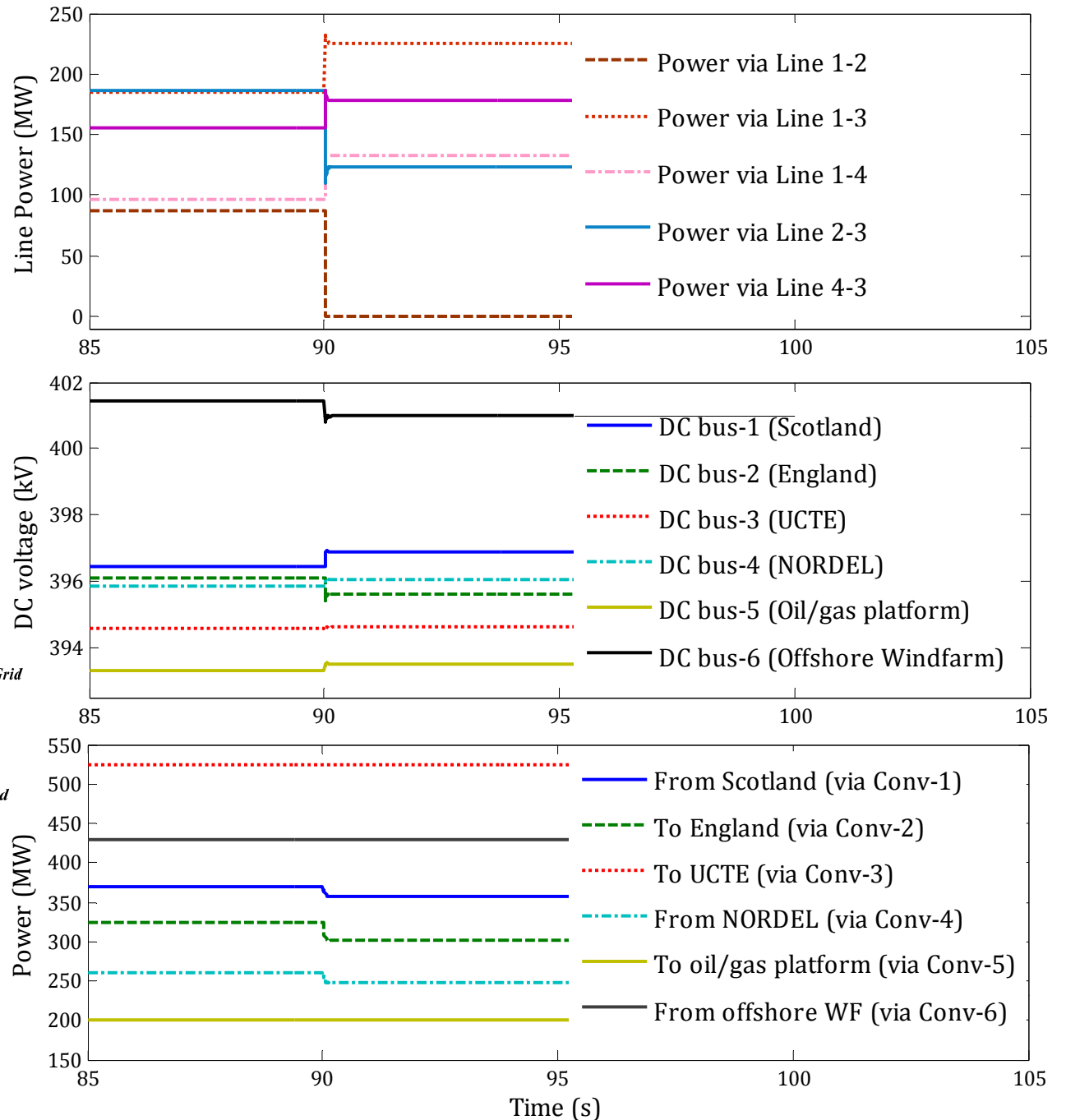
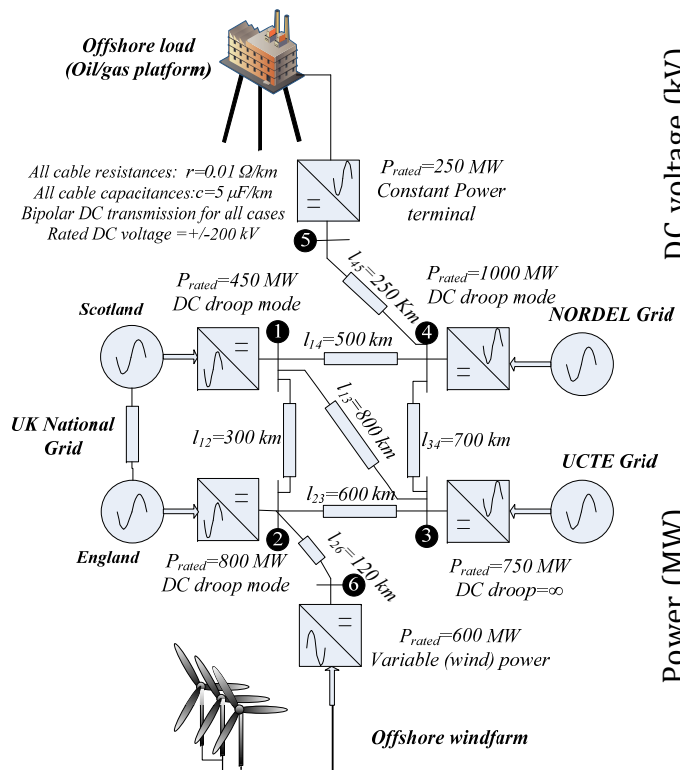
- Managing normal wind variations
- Outage of DC connections
- Outage of generation (wind farm tripping)
- Primary control response to ac grid contingency (exchange of primary reserves)
- Need for secondary control

# Variations of DC voltage with fluctuating wind power and DC droop control responses

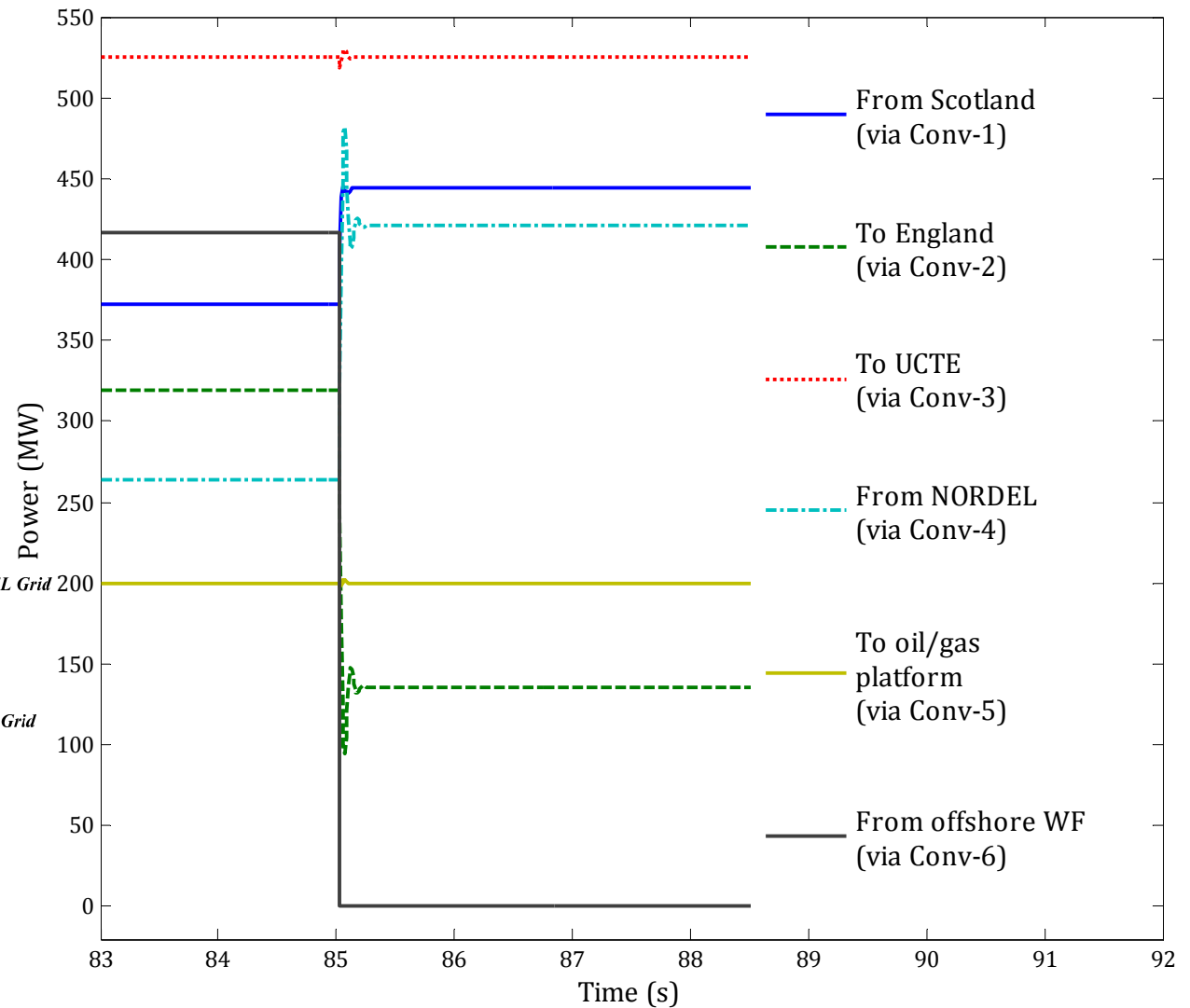
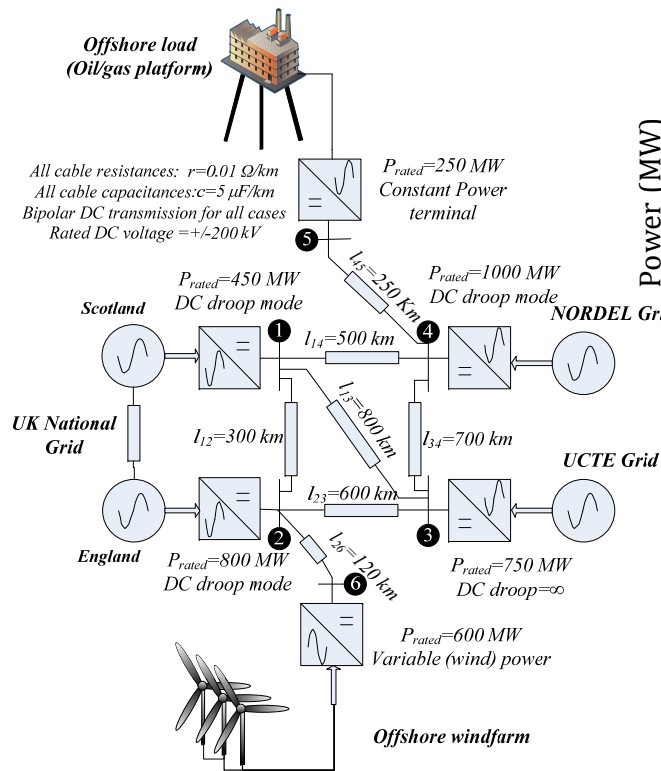


# Outage of DC line 1-2

Terminal-1 (Conv-1) continues to draw power from DC grid via lines 1-3 and 1-4 when line 1-2 is disconnected.

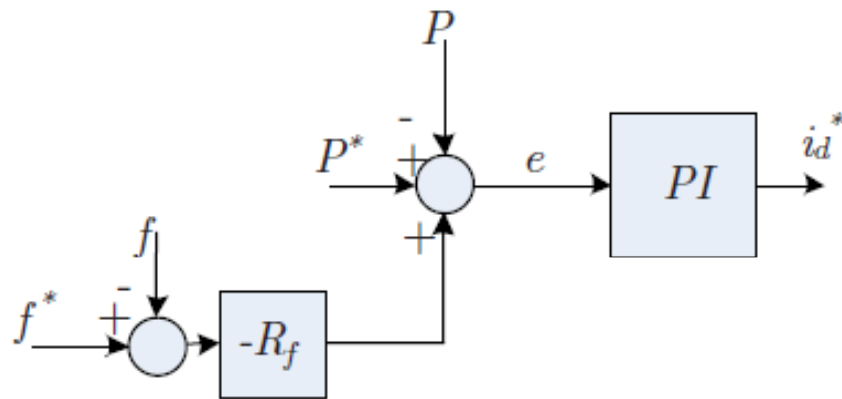


# Outage of connection to windfarm

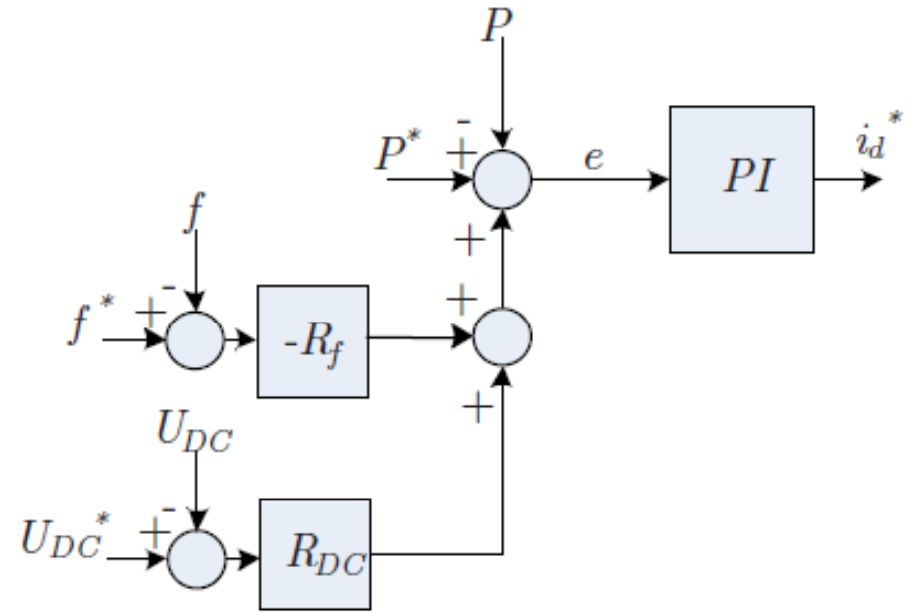


Terminals 1, 2 and 4 compensate for lost power flow from offshore wind farm.

# Frequency response enhancement of AC grids by VSC-HVDC



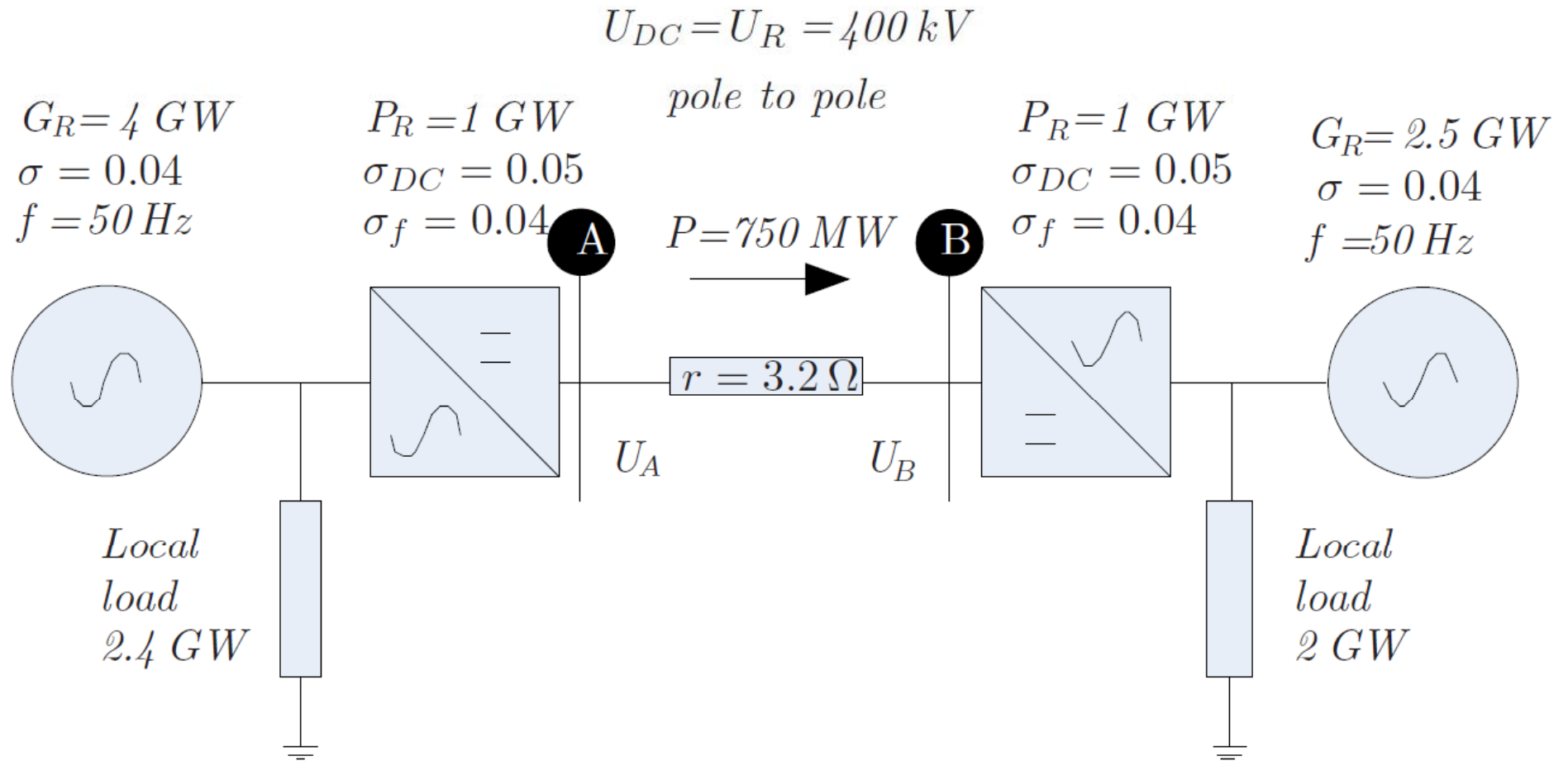
(a)



(b)

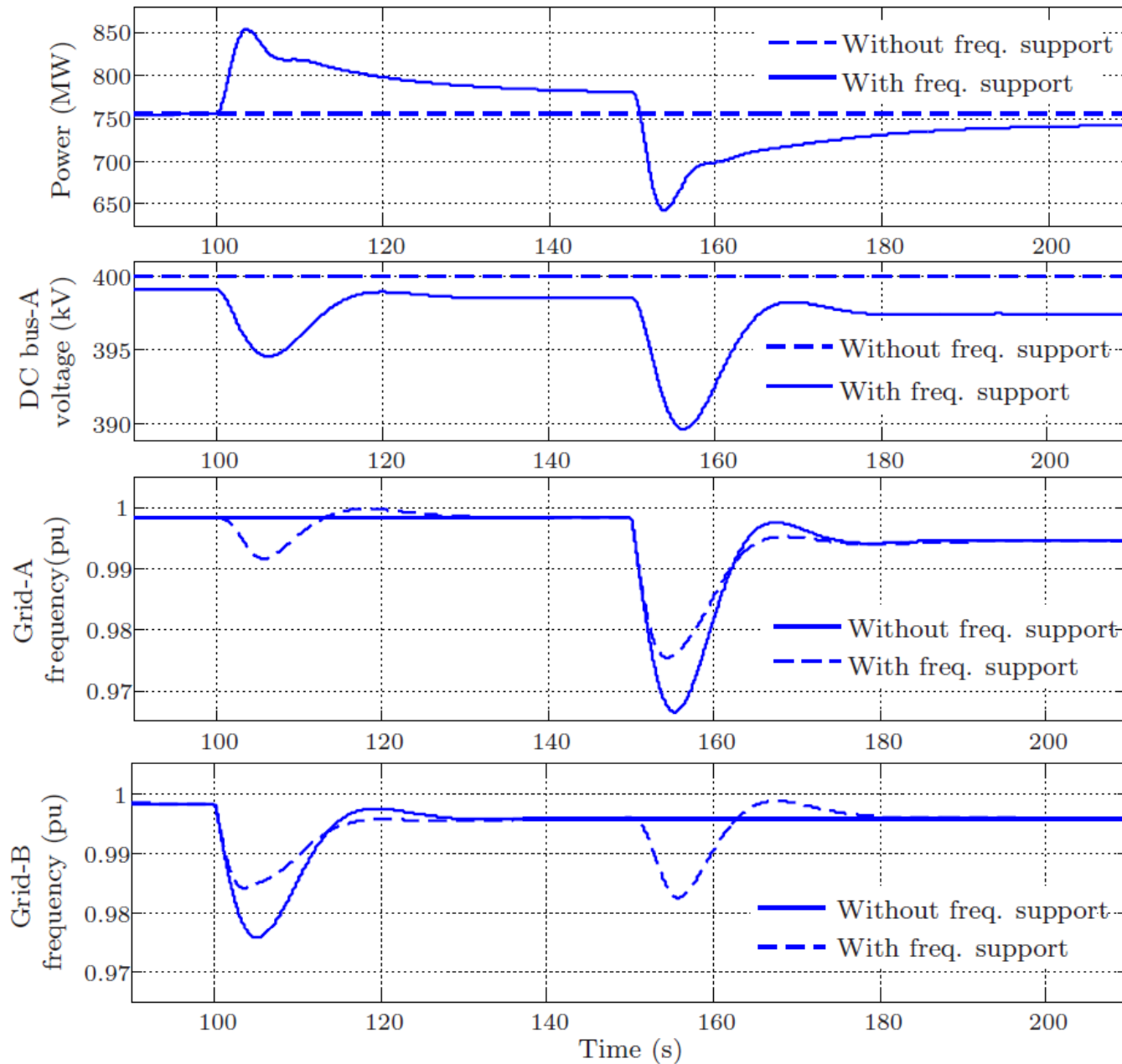
Frequency droop control implementation on VSC-HVDC with:  
 (a) constant power control (b) DC voltage droop control

# Frequency response enhancement example: two terminal VSC-HVDC

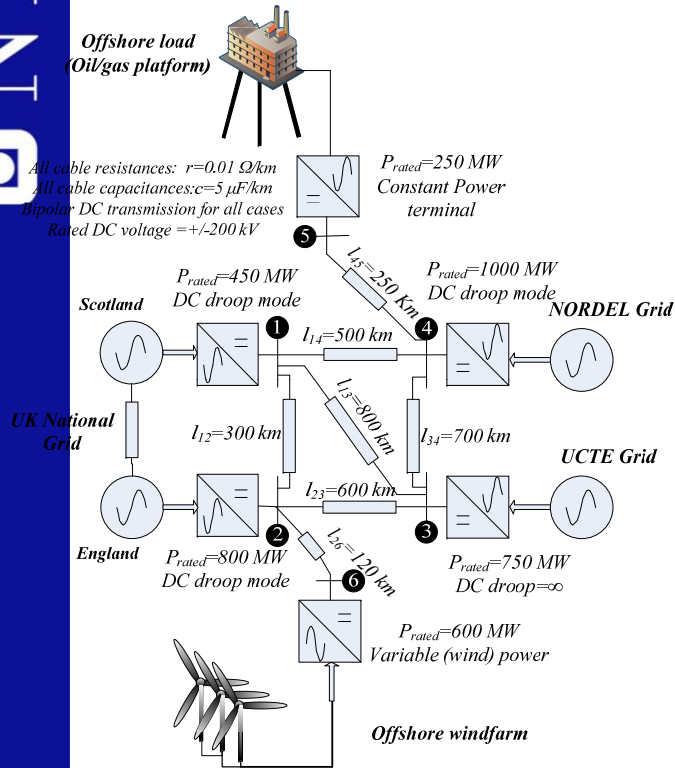




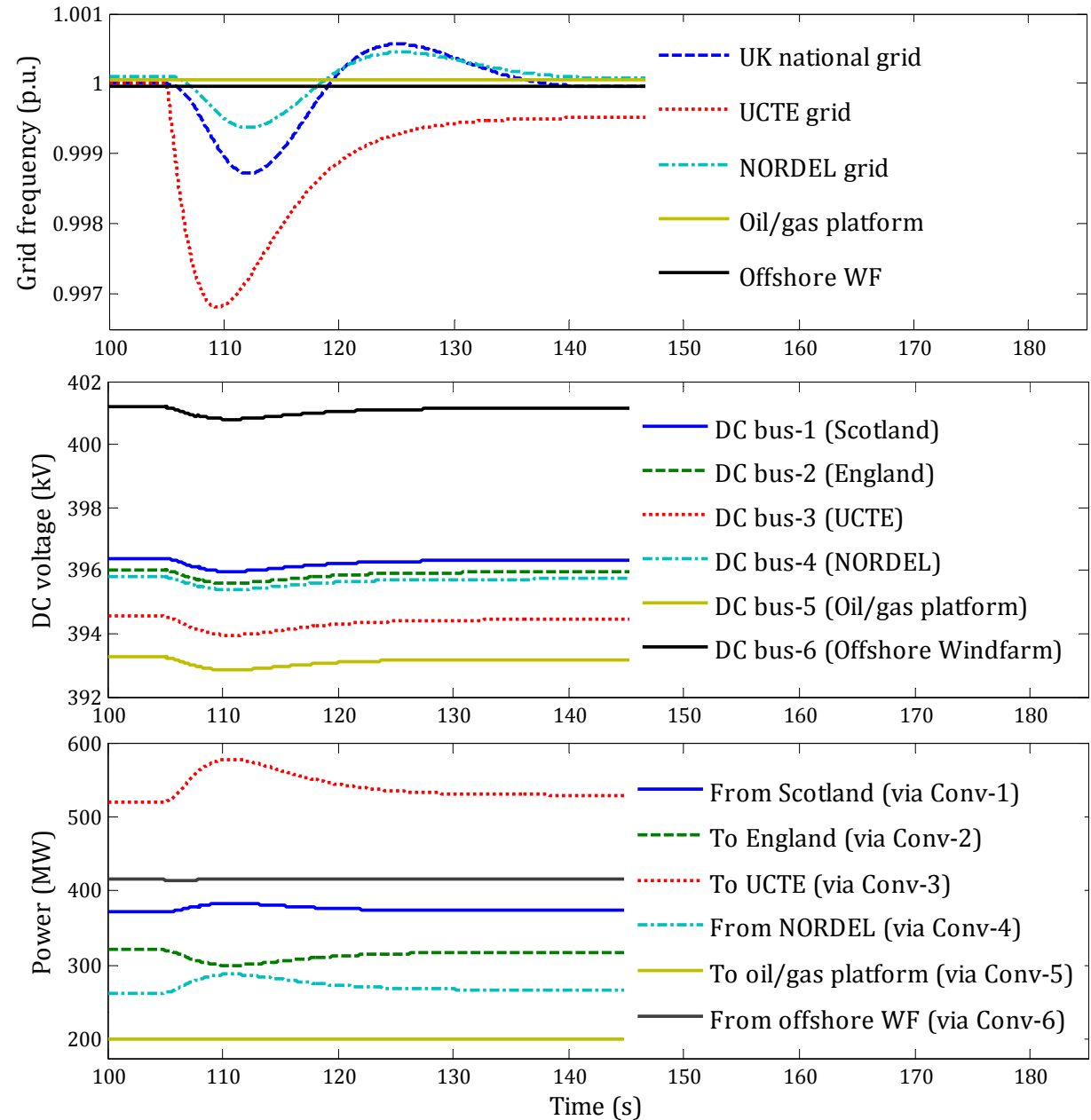
# Effect of frequency droop control (in VSC-HVDCs) on AC grid frequency responses



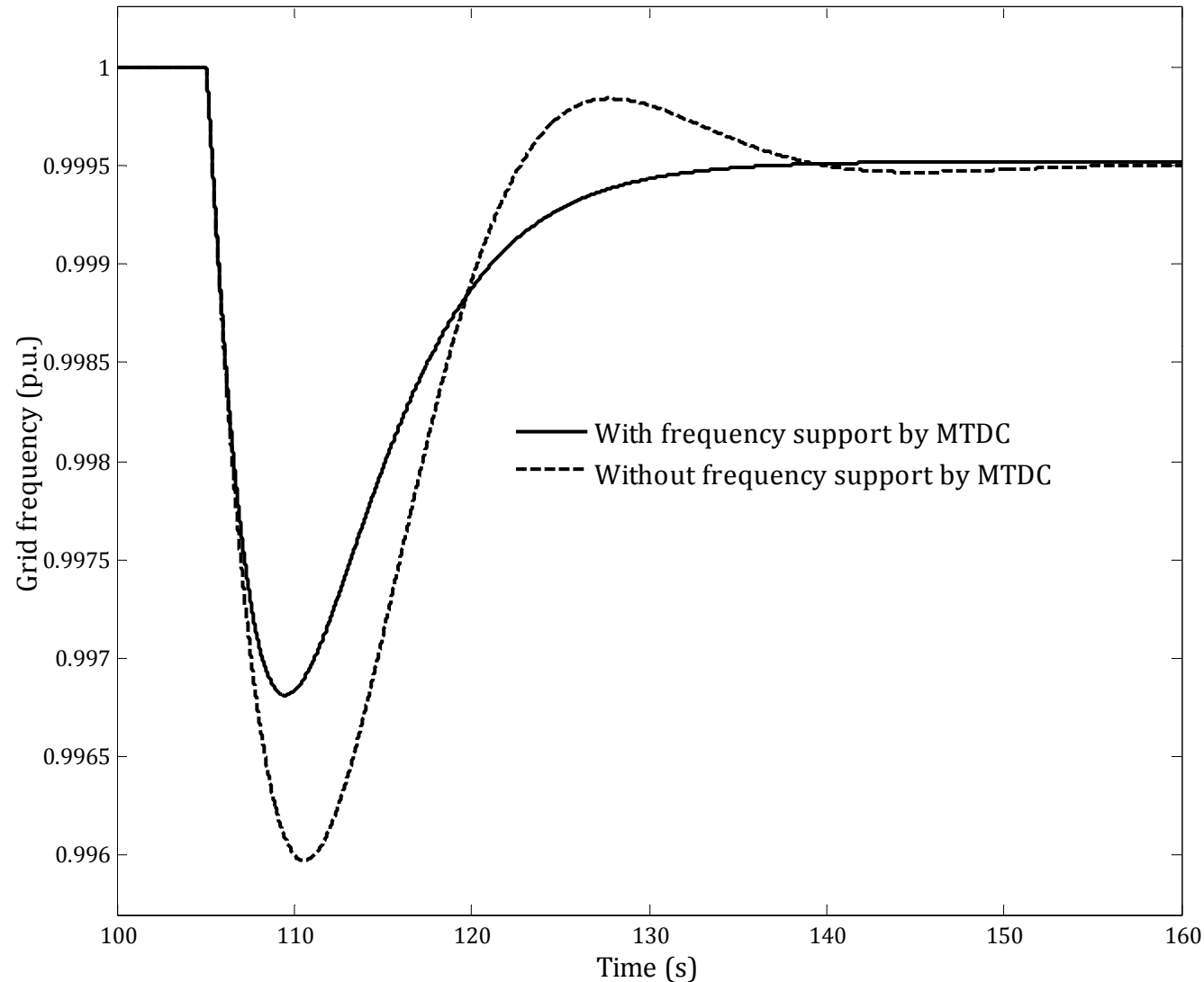
# Frequency response enhancement of AC grids by MTDC



UCTE grid frequency supported by NORDEL and UK (via two HVDC stations: one at England and the other in Scotland)



# Comparison of grid responses (UCTE grid): with and without frequency support from DC grid



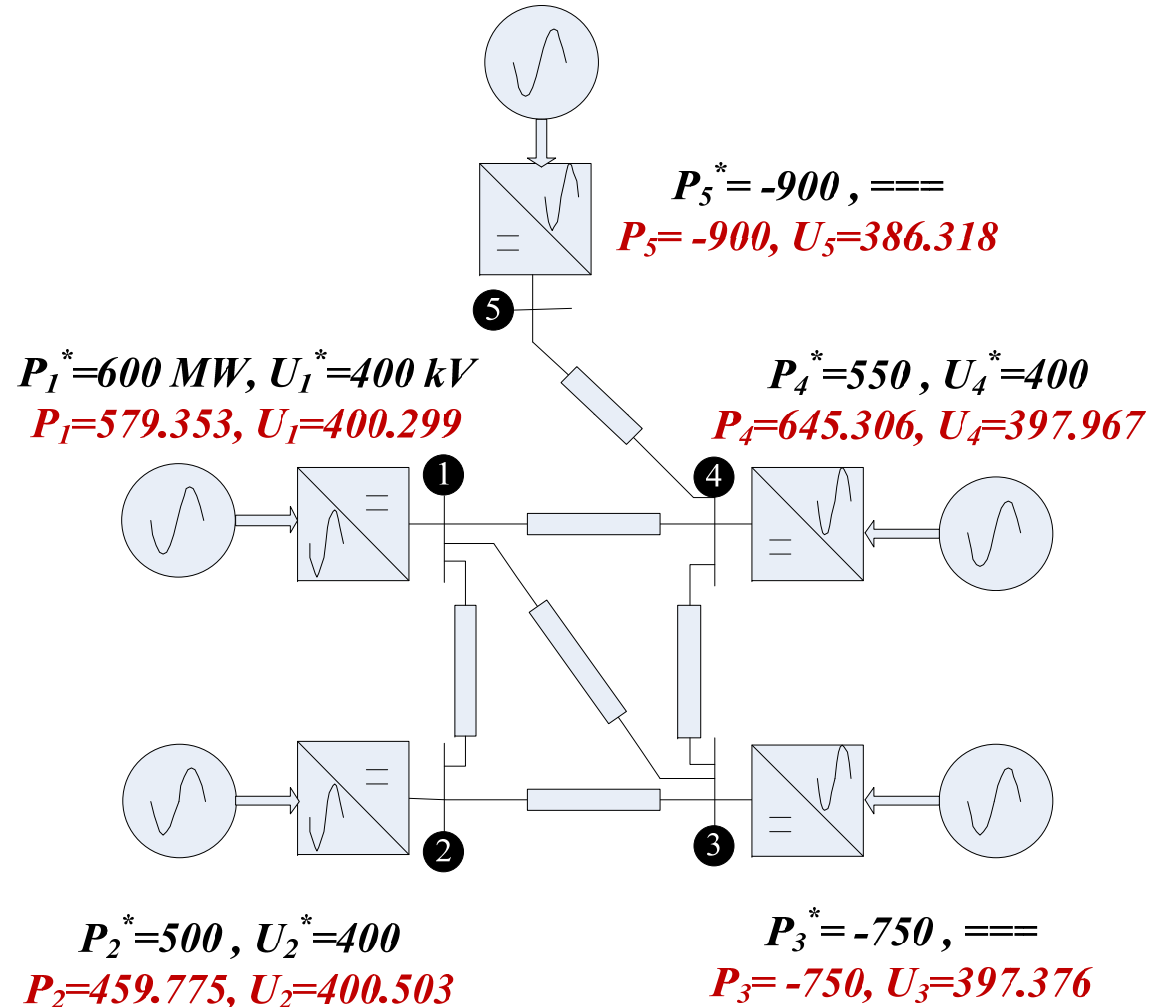
Frequency response improves with presence of frequency support from DC grid.

# Precise control of power flow

Schedule/ dispatch			Control type
Terminal No.	$P_{DC}$ (MW)	$U_{DC}$ (kV)	
1	600	-	Droop
2	-	400	Droop
3	-750	-	Fixed P
4	550	-	Droop
5	-900	-	Fixed P



Control references			Control type
Terminal No.	$P_{DC}$ (MW)	$U_{DC}$ (kV)	
1	600	400	Droop
2	500	400	Droop
3	-750	400	Fixed P
4	550	400	Droop
5	-900	400	Fixed P



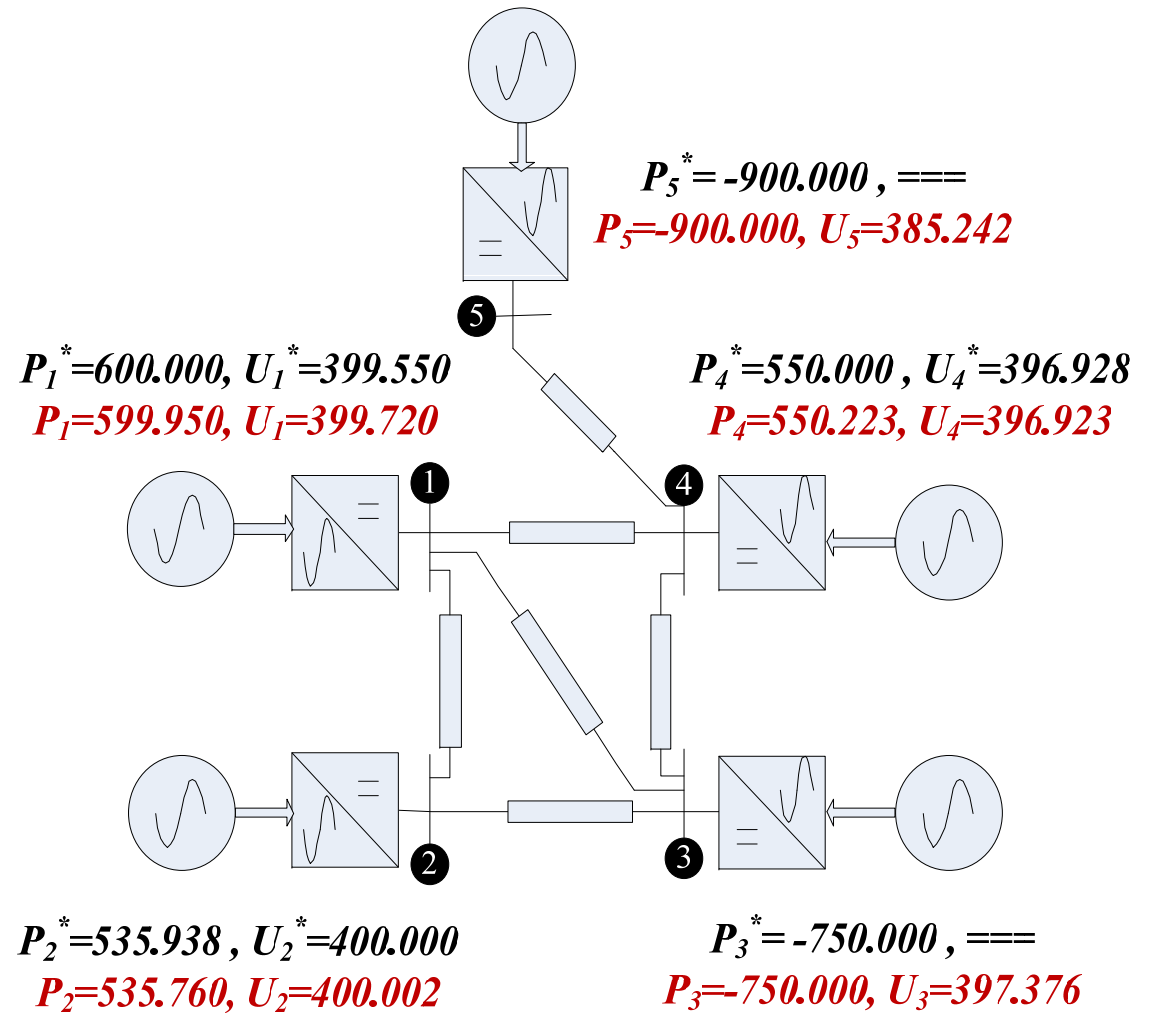
**Not precise!**

# Cntd...

Schedule/ dispatch			Control type
Terminal No.	$P_{DC}$ (MW)	$U_{DC}$ (kV)	
1	600	-	Droop
2	-	400	Droop
3	-750	-	Fixed P
4	550	-	Droop
5	-900	-	Fixed P

↓  
**DC Power flow analysis**  
 ↓

Control references			Control type
Terminal No.	$P_{DC}$ (MW)	$U_{DC}$ (kV)	
1	600.00	399.550	Droop
2	535.94	400.000	Droop
3	-750.00	396.613	Fixed P
4	550.00	396.928	Droop
5	-900.00	385.247	Fixed P

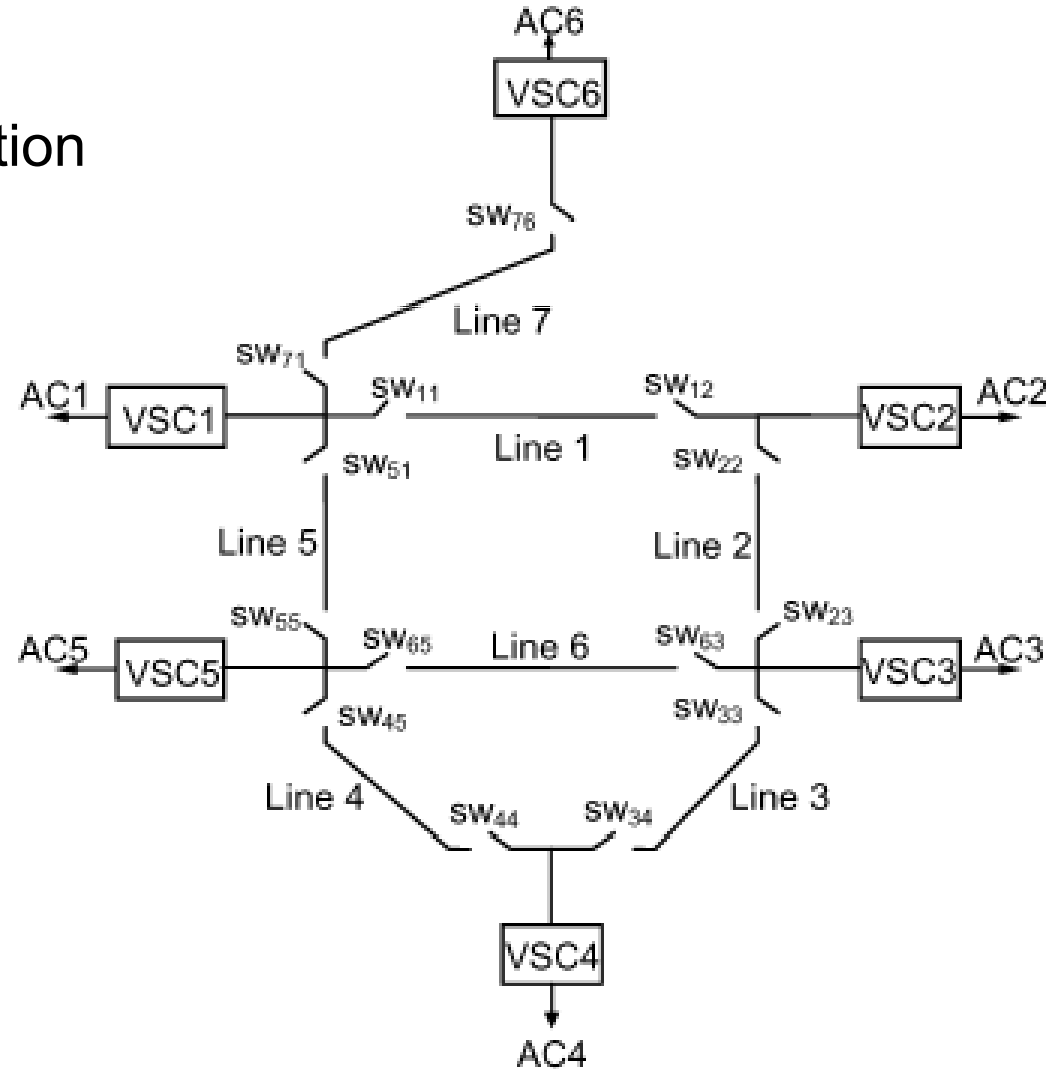


## Precise!

(Desired power flow achieved)

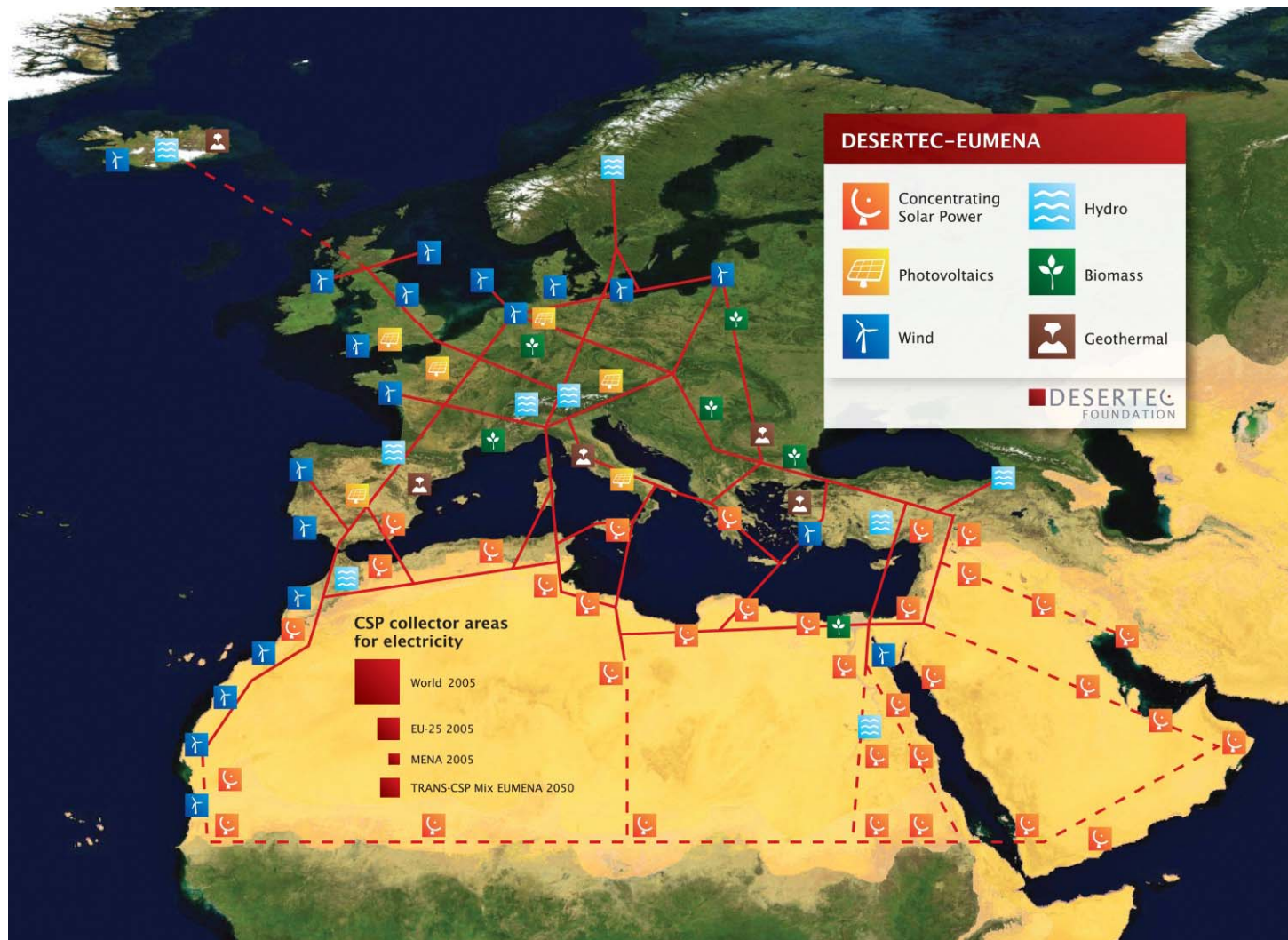
# Future works on MTDC

- Protection schemes
- Fault detection and localization algorithms
- Communication based (?)



# Future works...

Impact of wide area MTDC  
(Stability, operational, ...)



**Thank you!**